

Contribution to HiLiftPW-3

Scott Wurst, Riccardo Balin, Ryan Skinner, and
Kenneth E. Jansen,

University of Colorado Boulder

PID 035

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Summary of cases completed: PHASTA, Committee, Spalart-Allmaras

Case	Alpha=8, Fully turb, grid study	Alpha=16, Fully turb, grid study	Other
1a (full gap)	Yes	Yes	B1 Vgrid C/M/F
1b (full gap w adaption)	no	no	
1c (partial seal)	no	no	
1d (partial seal w adaption)	no	no	
Other			

Case	Polar, Fully turb	Polar, specified transition	Polar, w transition prediction	Other
2a (no nacelle)	Yes	no	Yes	C1 Vgrid M
2b (no nacelle w adaption)	no	no	no	
2c (with nacelle)	Yes	no	Yes	C1 Vgrid M
2d (with nacelle w adaption)	no	no	no	
Other				

Case	2D Verification study	Other
3	Yes	
Other		

Summary of cases completed: PHASTA, Simmetrix, Spalart-Allmaras

Case	Alpha=8, Fully turb, grid study	Alpha=16, Fully turb, grid study	Other
1a (full gap)	Yes	Yes	C/M
1b (full gap w adaption)	no	Yes	ongoing
1c (partial seal)	no	no	
1d (partial seal w adaption)	no	no	
Other			

Geometry Model	Grid Type	Grid Level	Nodes	BFaces	Volume Cells
HLCRM-Full Gap	Unstructured Tetrahedra	Coarse	8.0 M	482 K	46.4 M
		Medium	22.4 M	1.27 M	132.4 M

- Simmetrix mesh designed for adaptivity
 - Generated against native CAD (Parasolid kernel)
 - Medium Simmetrix mesh matches Medium B1
 - Coarse Simmetrix mesh doubles surface edge size but keeps wall normal distribution of medium B1.
 - Also some refinement of corners
 - Still comparable size (e.g., B1 sizes are C=8.1, M=26.5, F=69.9 million nodes).

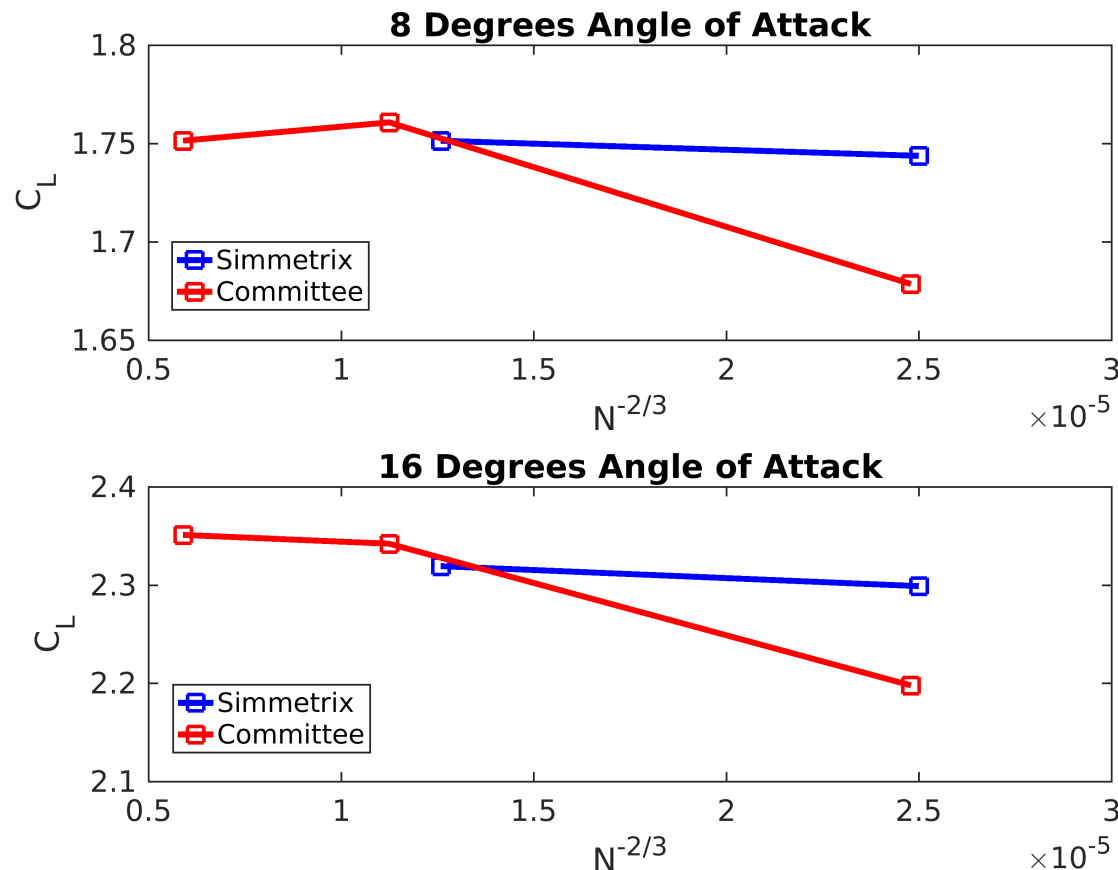
Summary of code and numerics used

- Parallel Hierarchic Stabilized Transient Analysis-PHASTA
 - SUPG finite element method with hierarchic basis, $k \leq 4$
 - Spatial accuracy demonstrated $O(h^{k+1})$
 - Backward Euler and second order generalized α time integration
 - Compressible and incompressible formulations
 - Scaled to more than 3M processes
 - Adaptivity linked to SCOREC/core and Simmetrix Inc. workflows to allow anisotropic boundary layer adaptivity
 - Results today are $k=1$, second order accurate in space
- RANS, URANS, and DDES completed on HiLiftPW2, DLR-F11. References:
 - Github.com/PHASTA and Github.com/SCOREC/core
 - AIAA Journal **53**,2,2014 Chitale et al.
 - AIAA 2014-{0749,2570,0117}, 2013-2445
 - AIAA-2017-3243 Vertical Tail Flow Control DDES Validation
 - AIAA-2017-3563 DLR-F11, HiLiftPW2 RANS, URANS, and DDES

CRM

Grid refinement effects - Forces

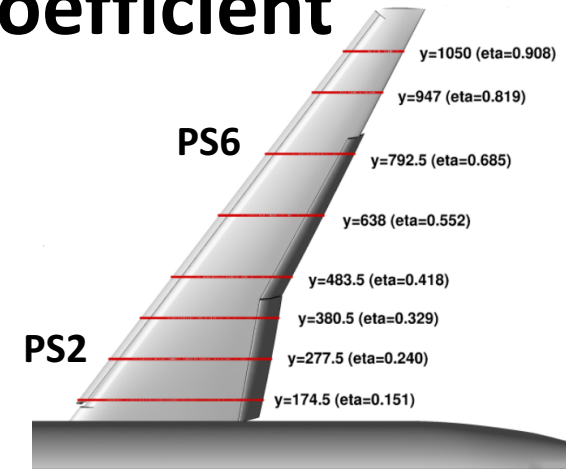
- Lift solution convergence, in terms of difference from fine grid result, was somewhat better for coarse grids at both AOA



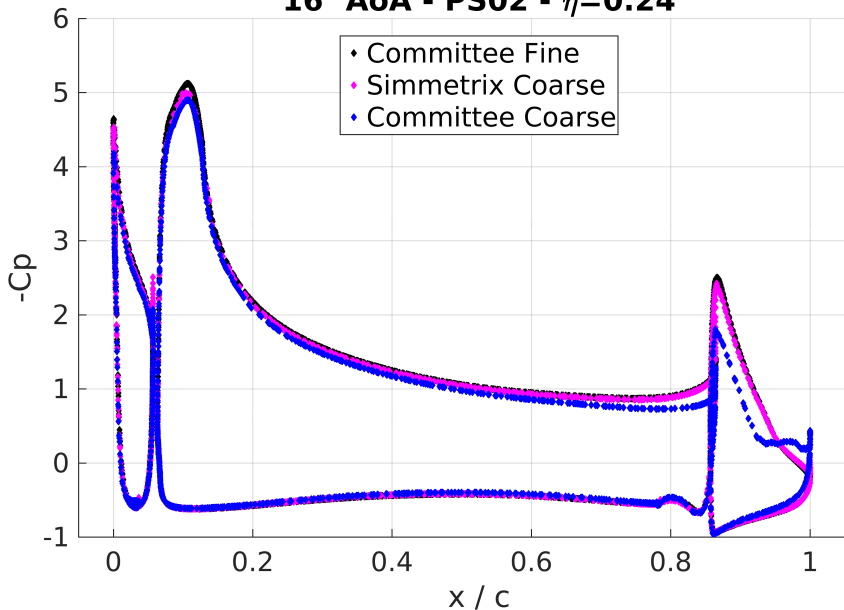
CRM

Grid refinement effects – Pressure coefficient

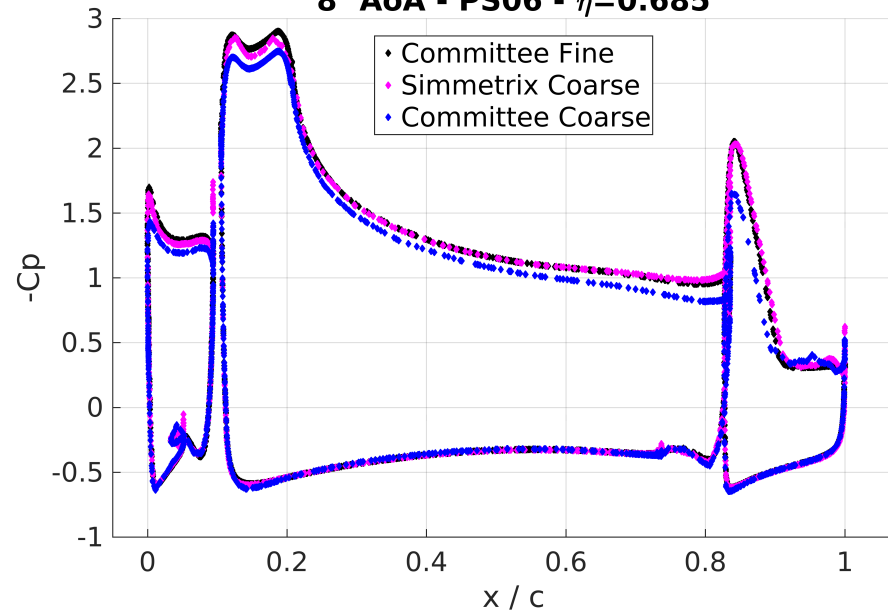
- Better coarse prediction of flap suggests B1 Coarse wall normal distribution likely the largest error source



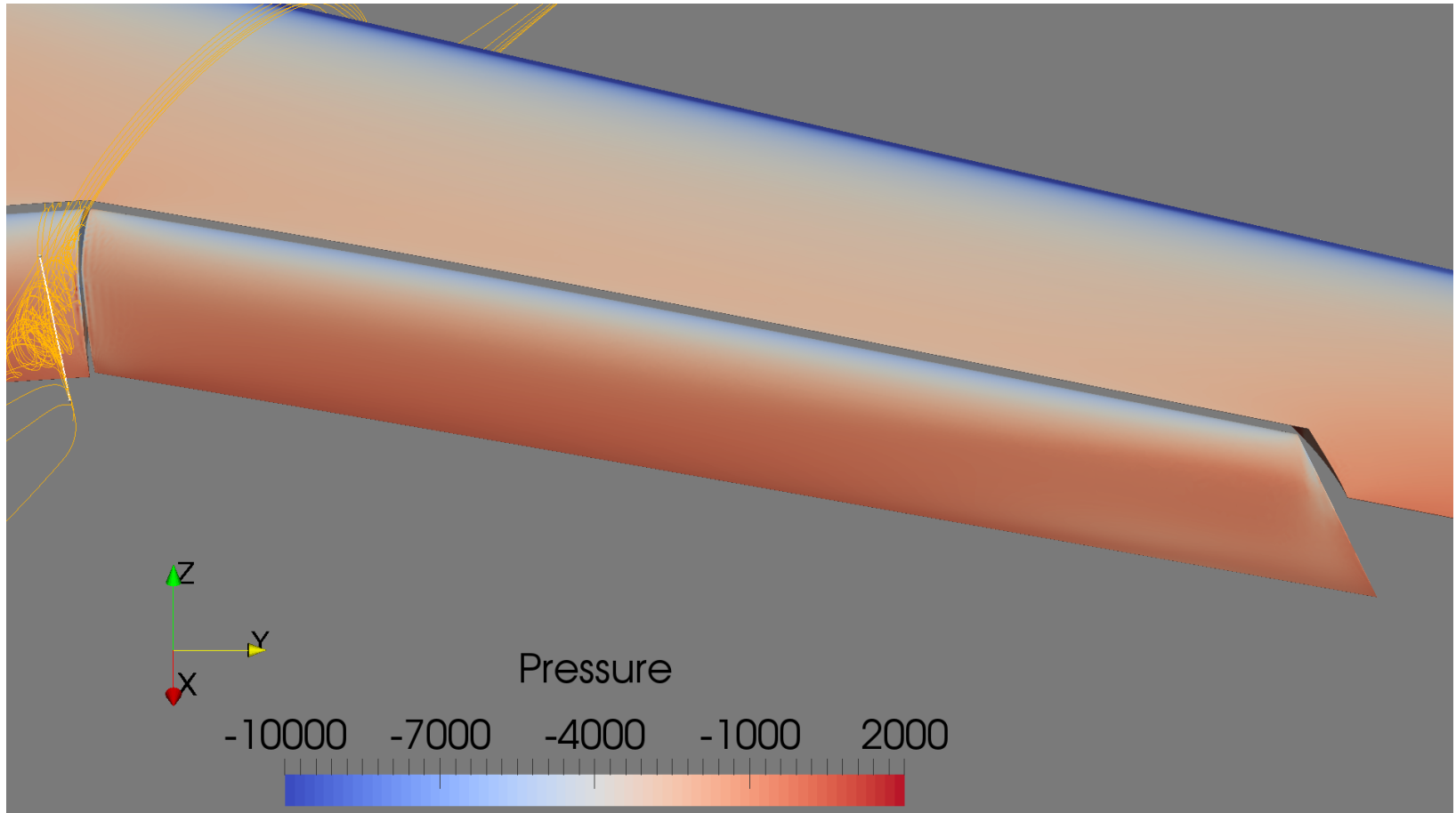
16° AoA - PS02 - $\eta=0.24$



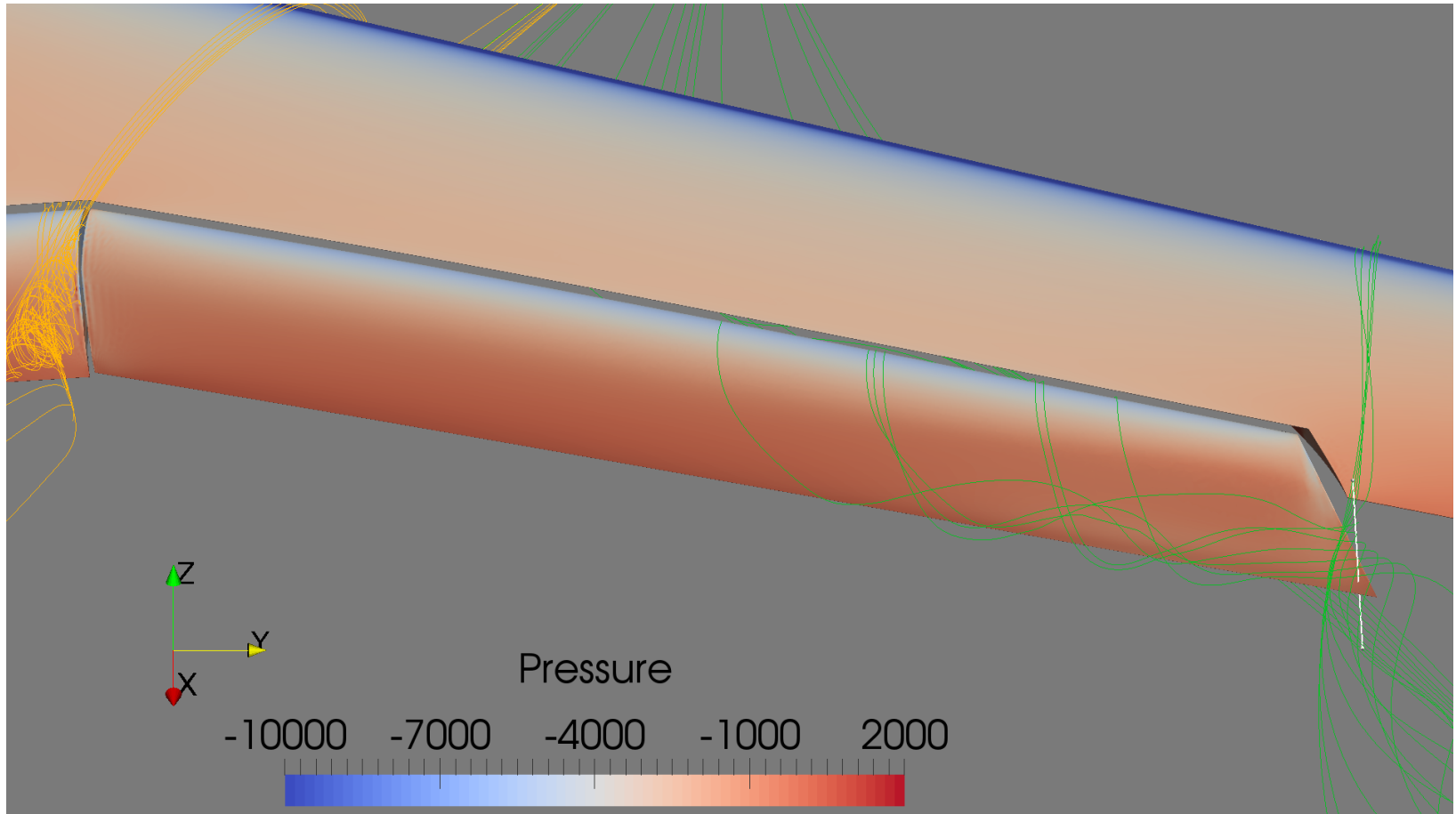
8° AoA - PS06 - $\eta=0.685$



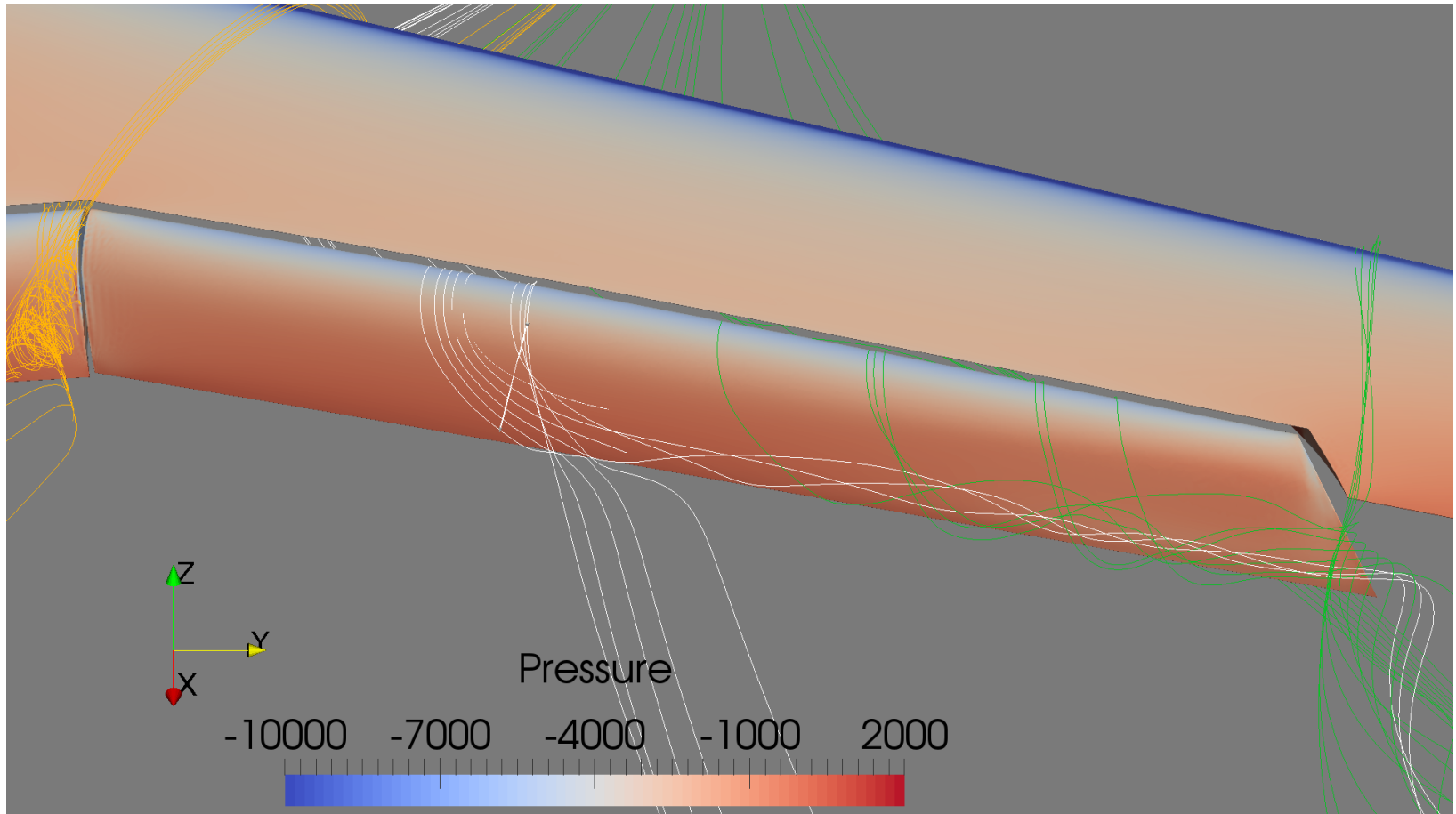
CRM Streamline Placement: Orange:Gap



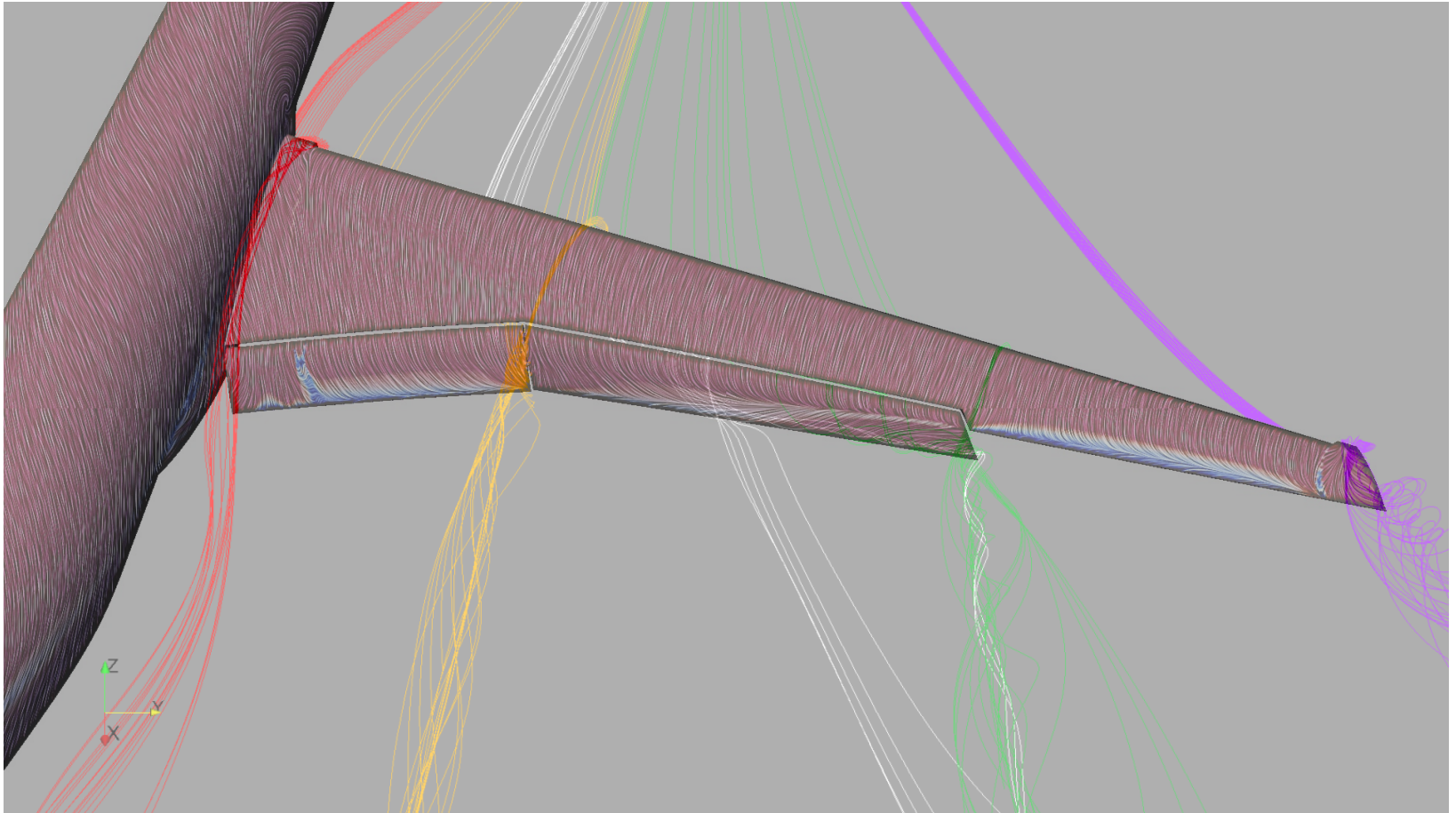
CRM Streamline Placement: Green: Flap Tip



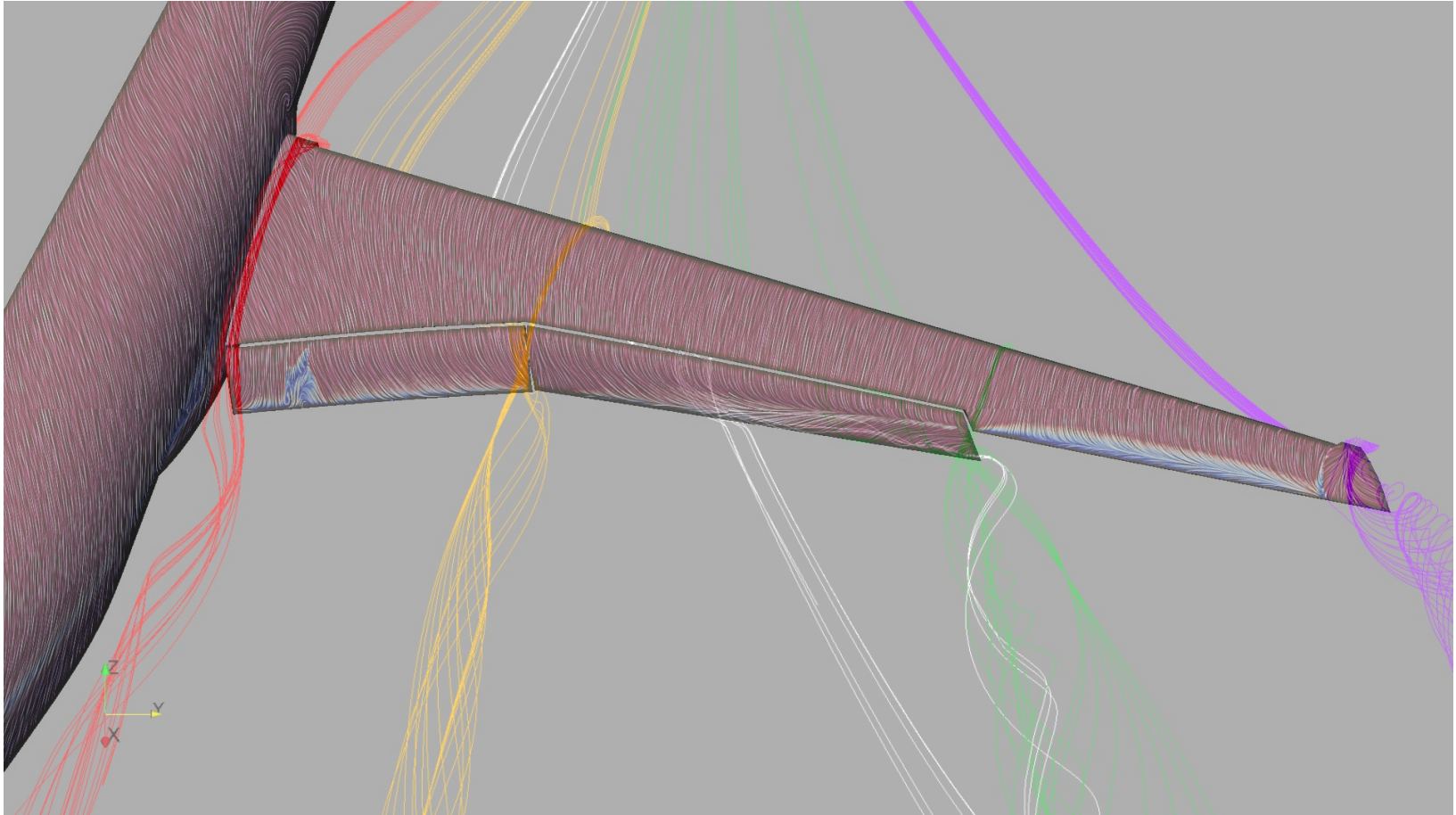
CRM Streamline Placement: White: Near Flap Surface



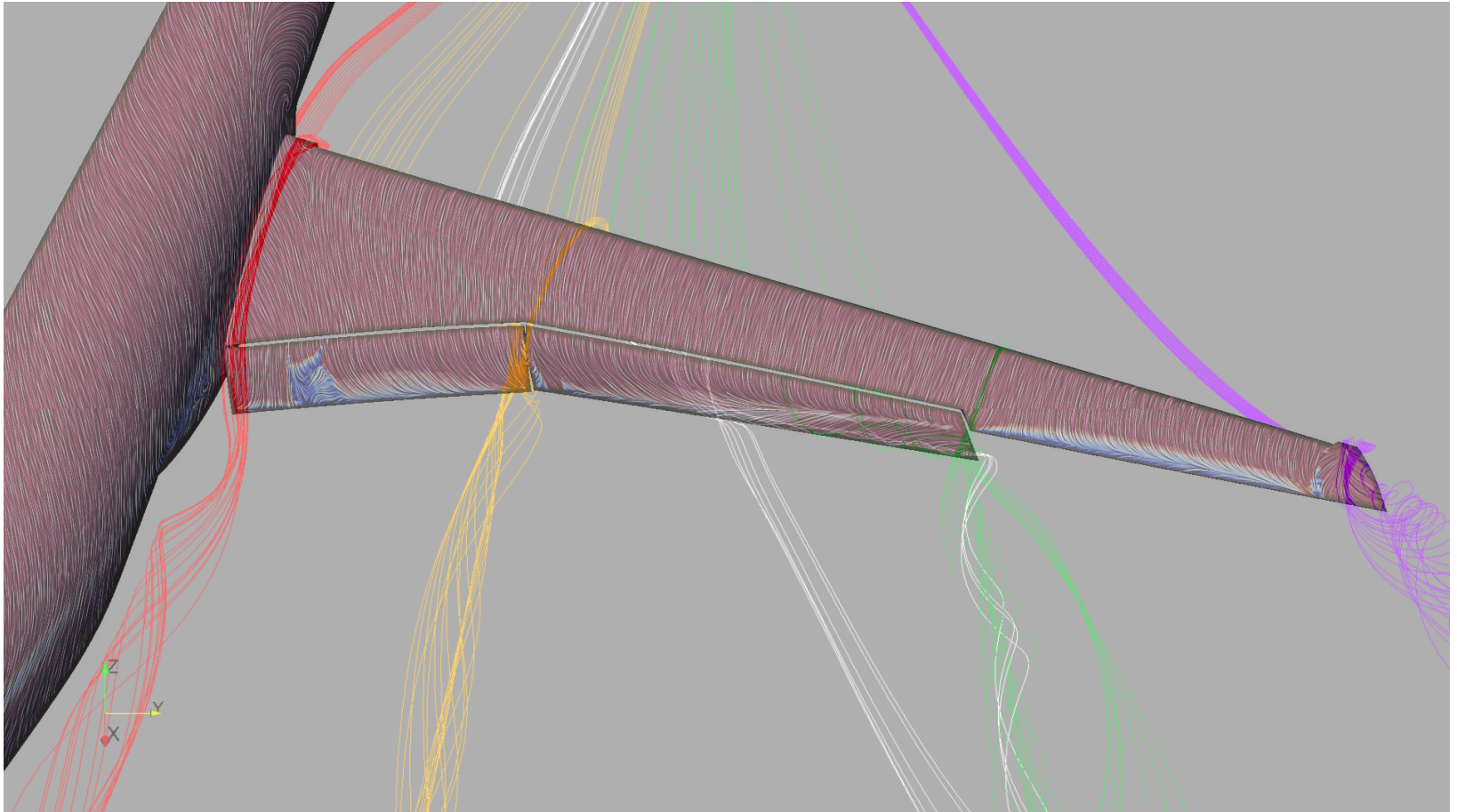
CRM Wall Shear Stress Streaks and Streamlines: Committee:Fine:16



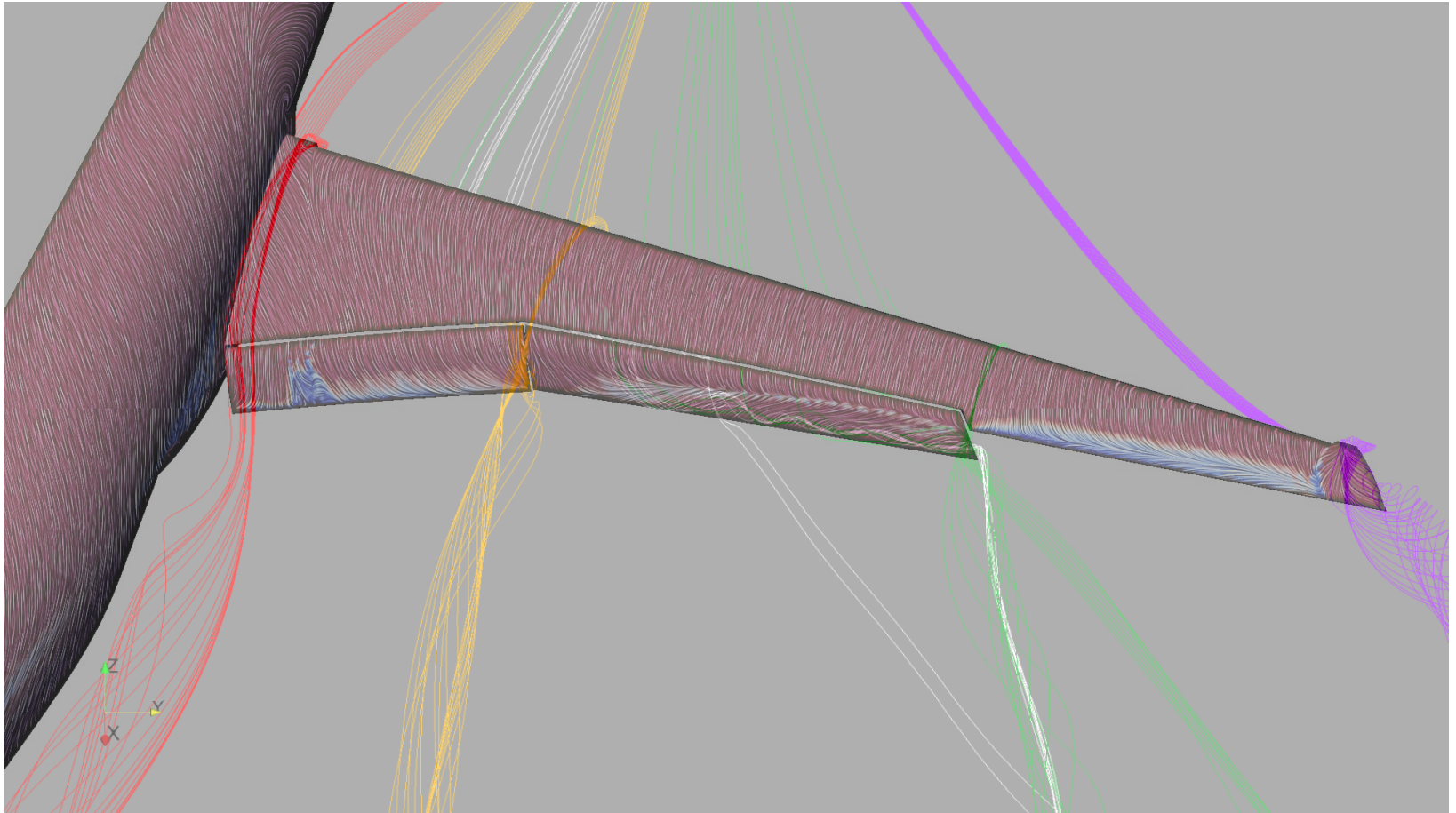
CRM Wall Shear Stress Streaks and Streamlines: Simmetrix:Medium:16



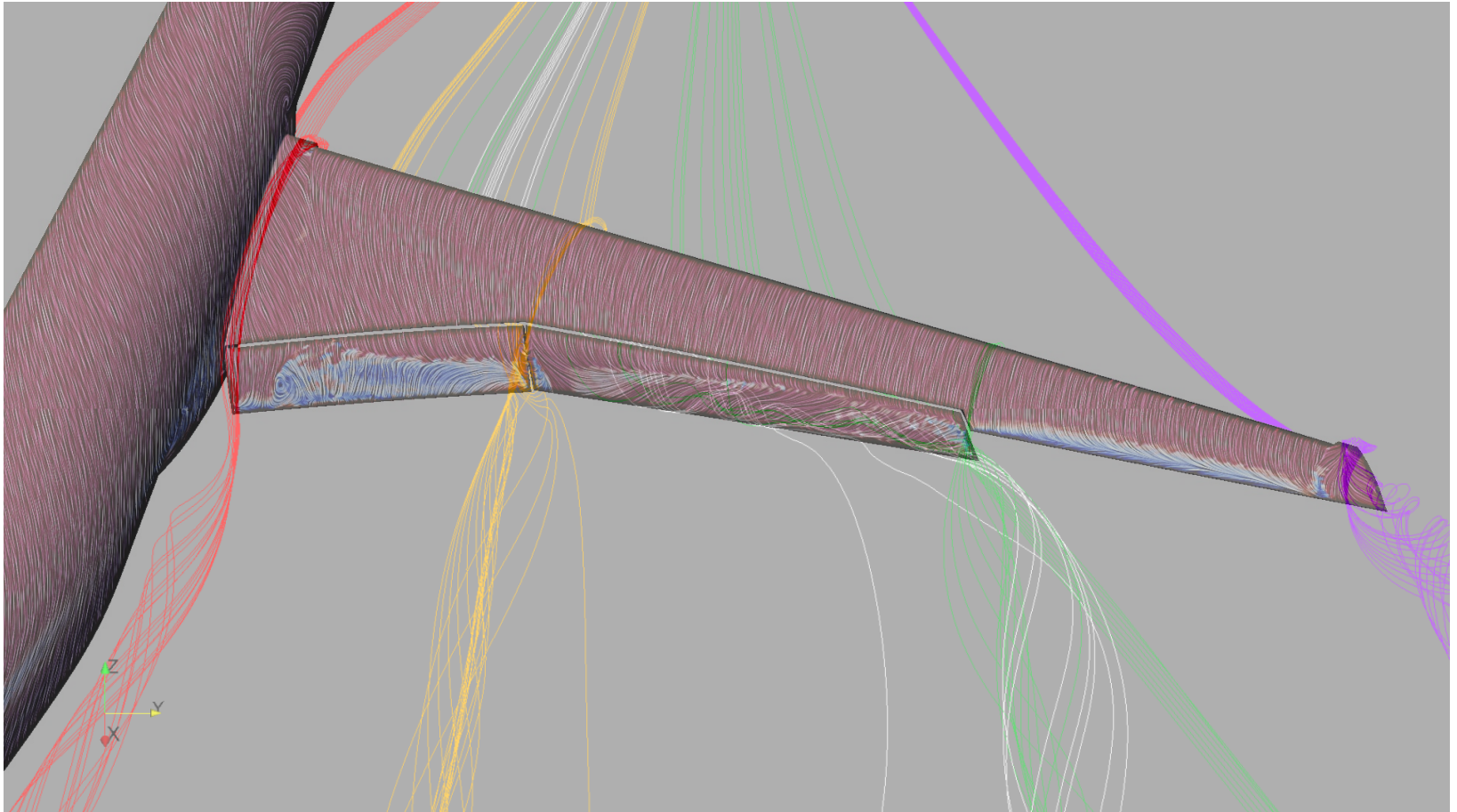
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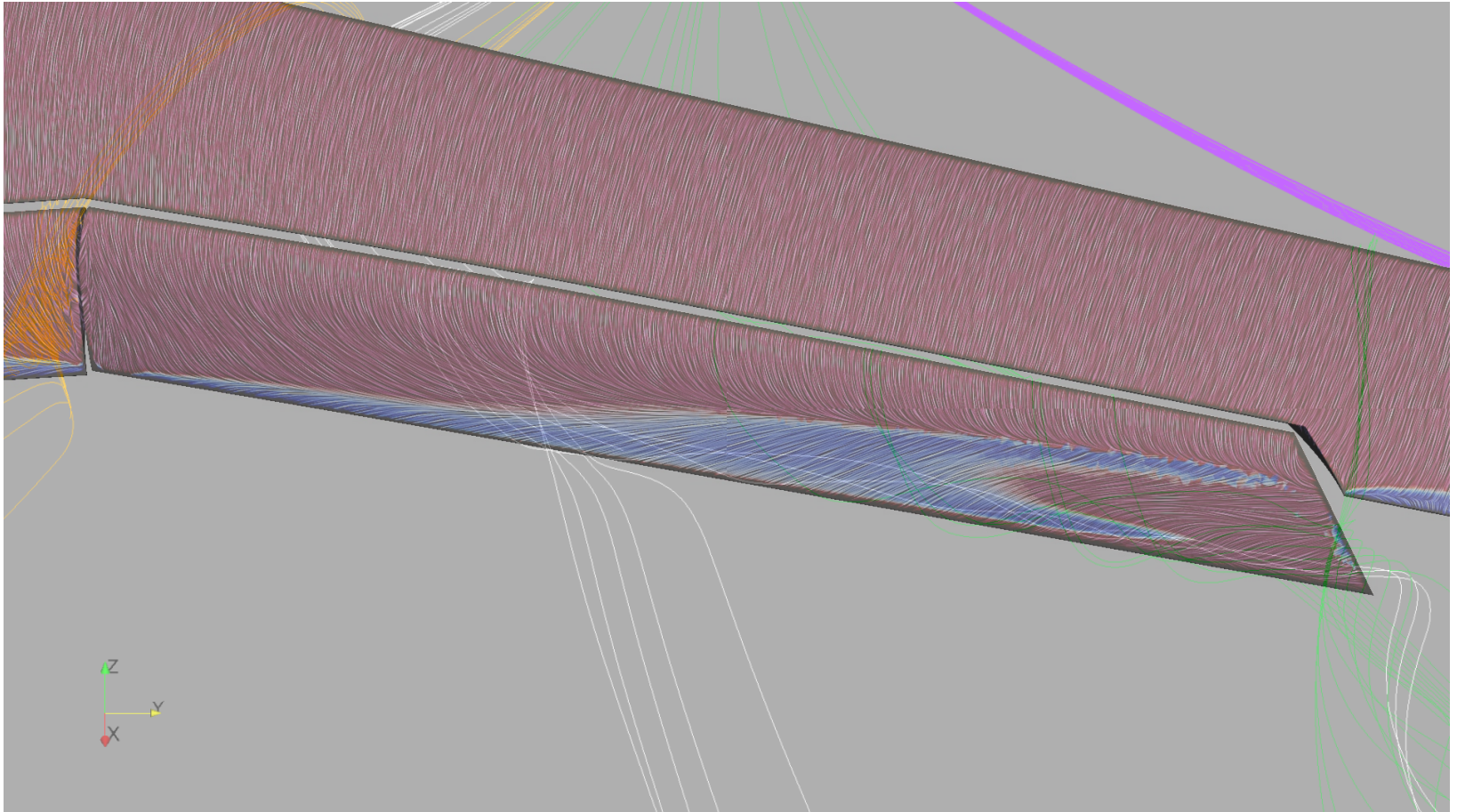
CRM Wall Shear Stress Streaks and Streamlines: Simmetrix:Coarse:16



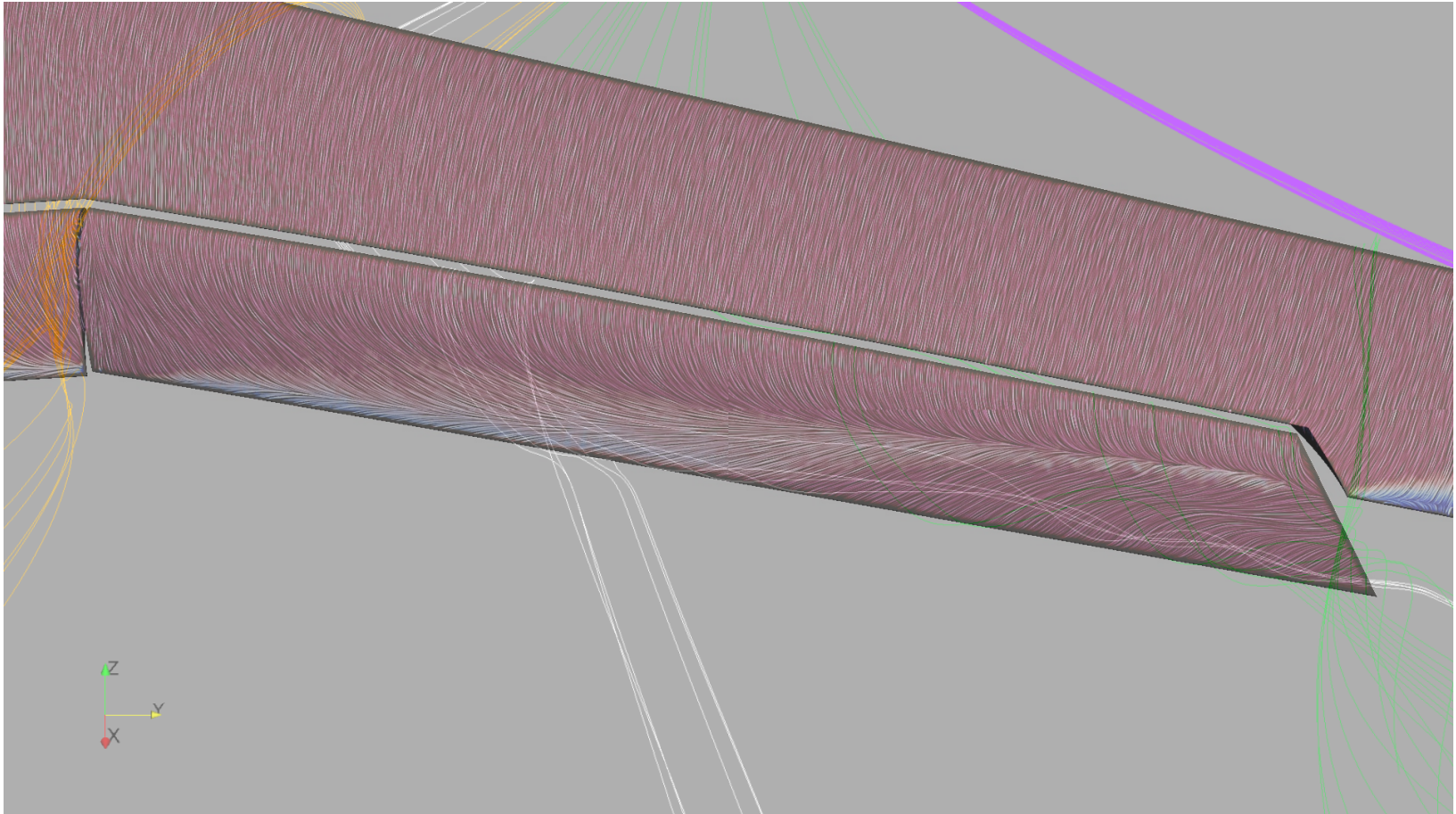
CRM Wall Shear Stress Streaks and Streamlines: Committee:Coarse:16



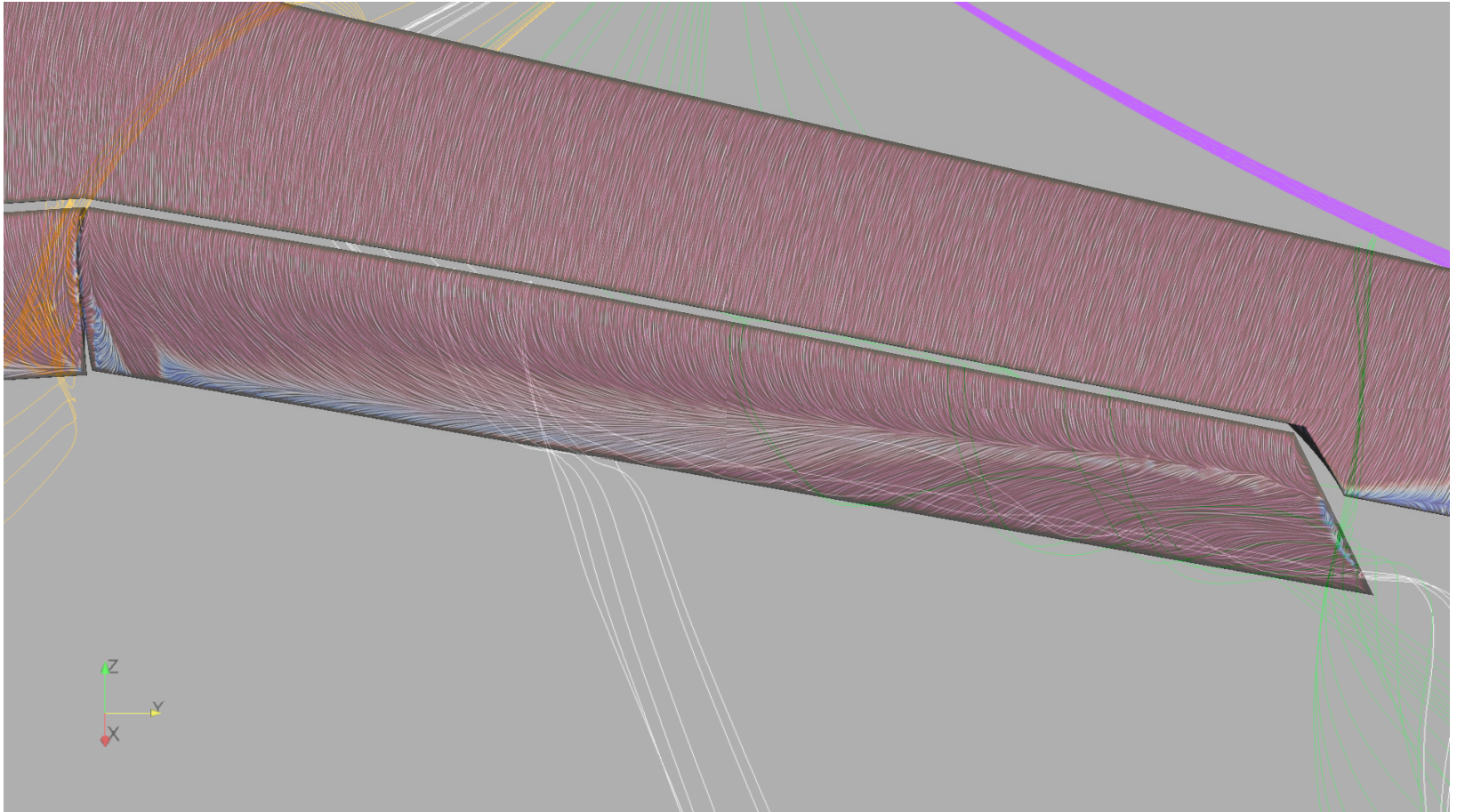
CRM Wall Shear Stress Streaks and Streamlines: Committee:Fine:16



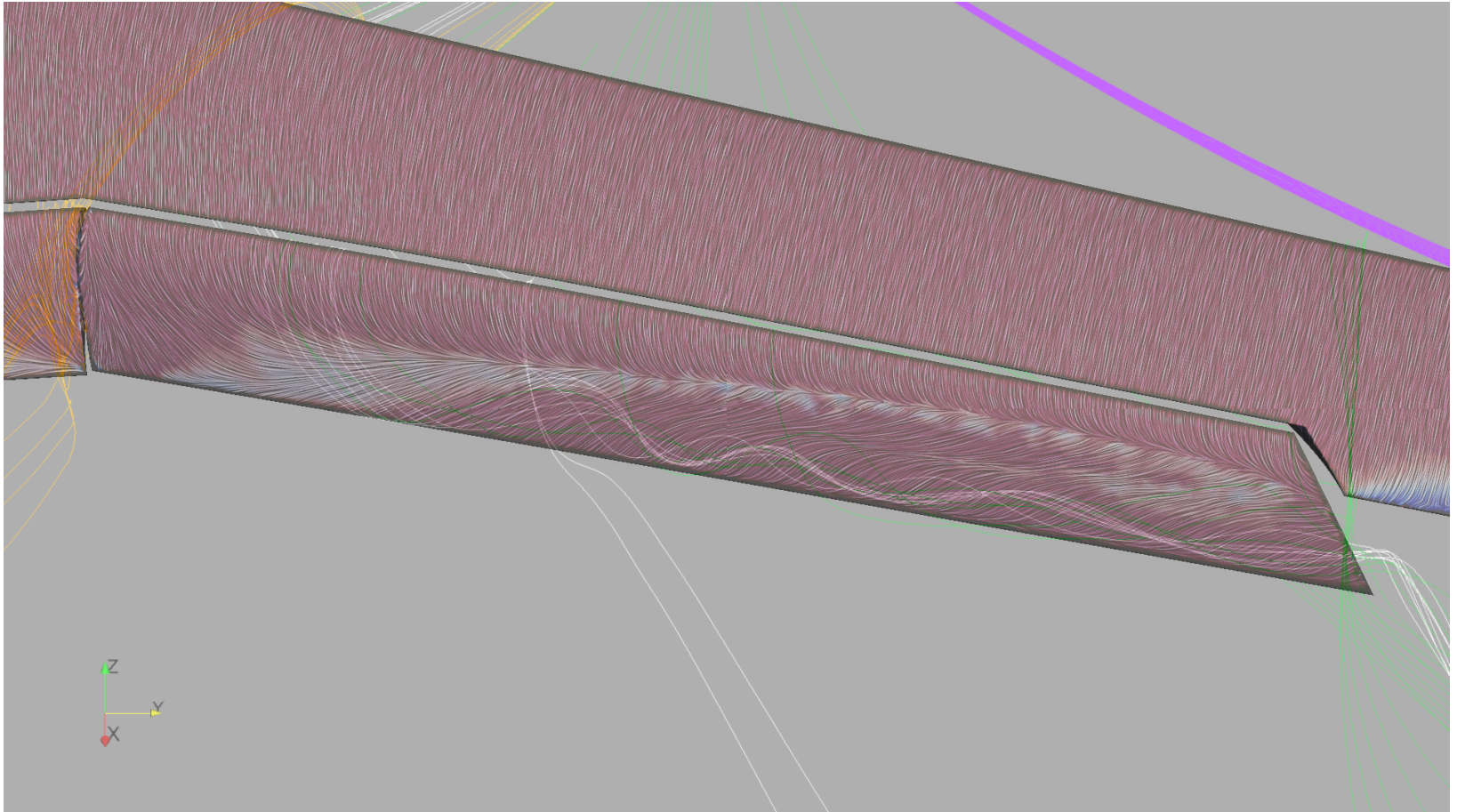
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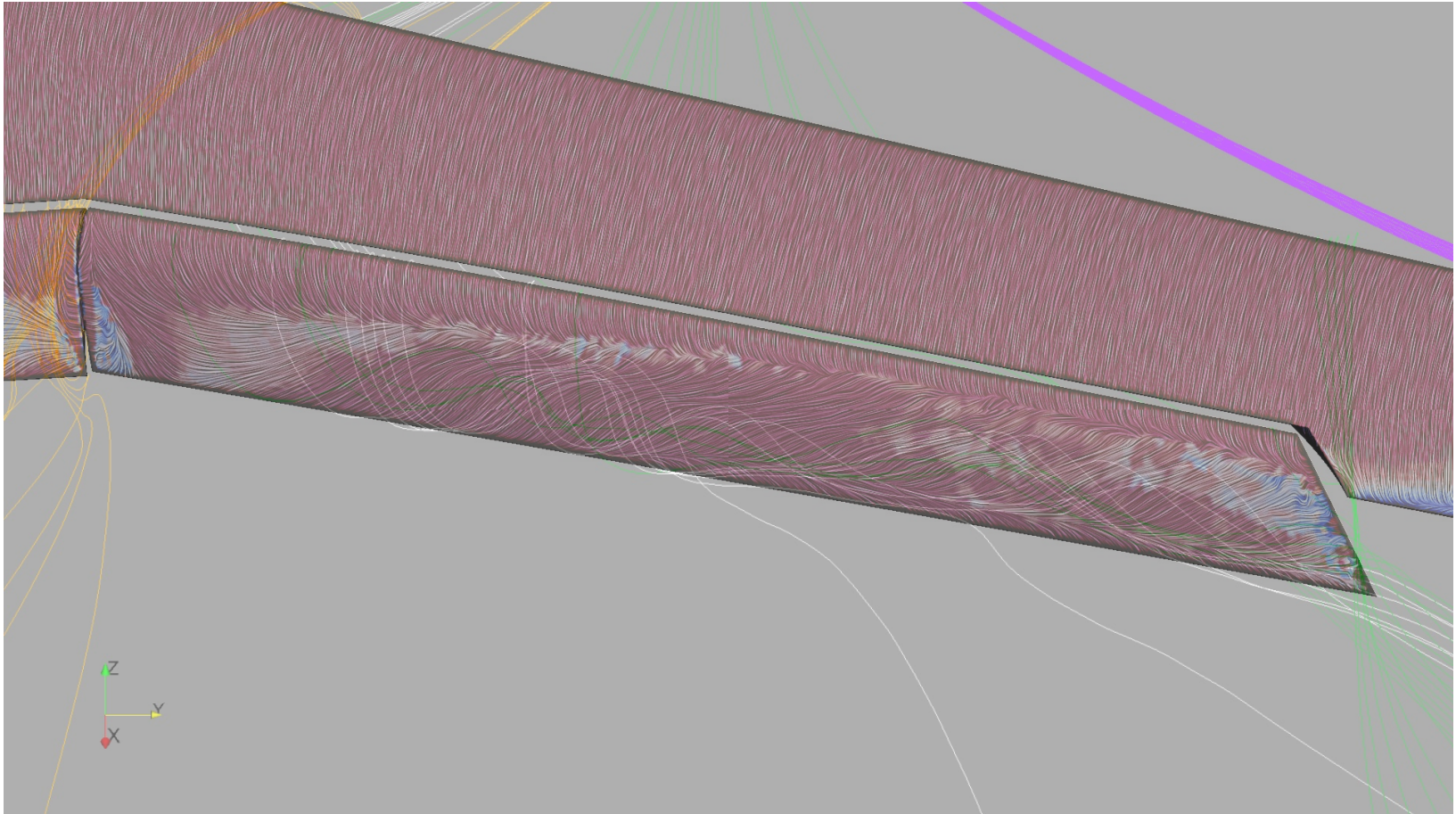
CRM Wall Shear Stress Streaks and Streamlines: Committee:Medium:16



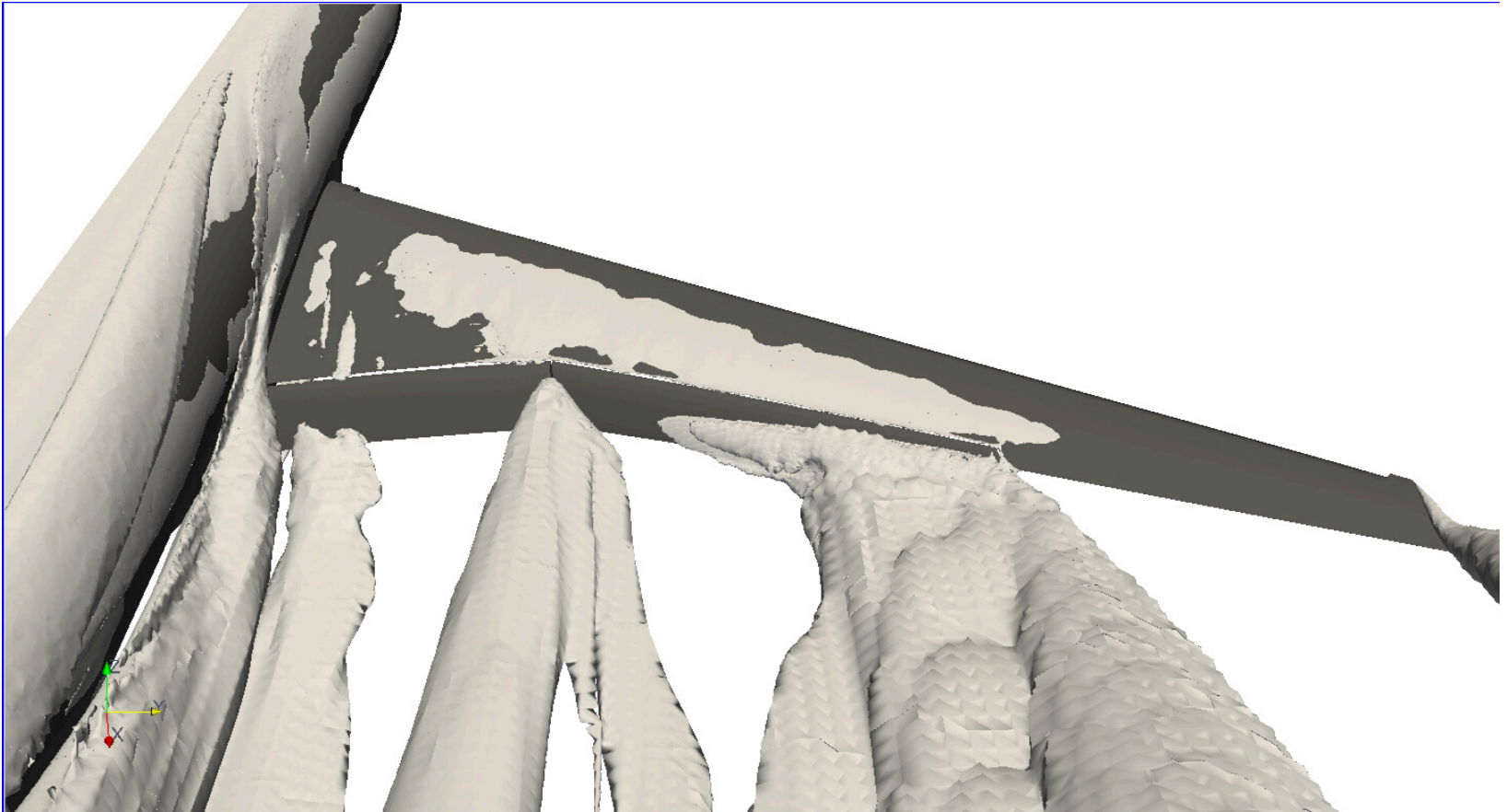
CRM Wall Shear Stress Streaks and Streamlines: Simmetrix:Coarse:16



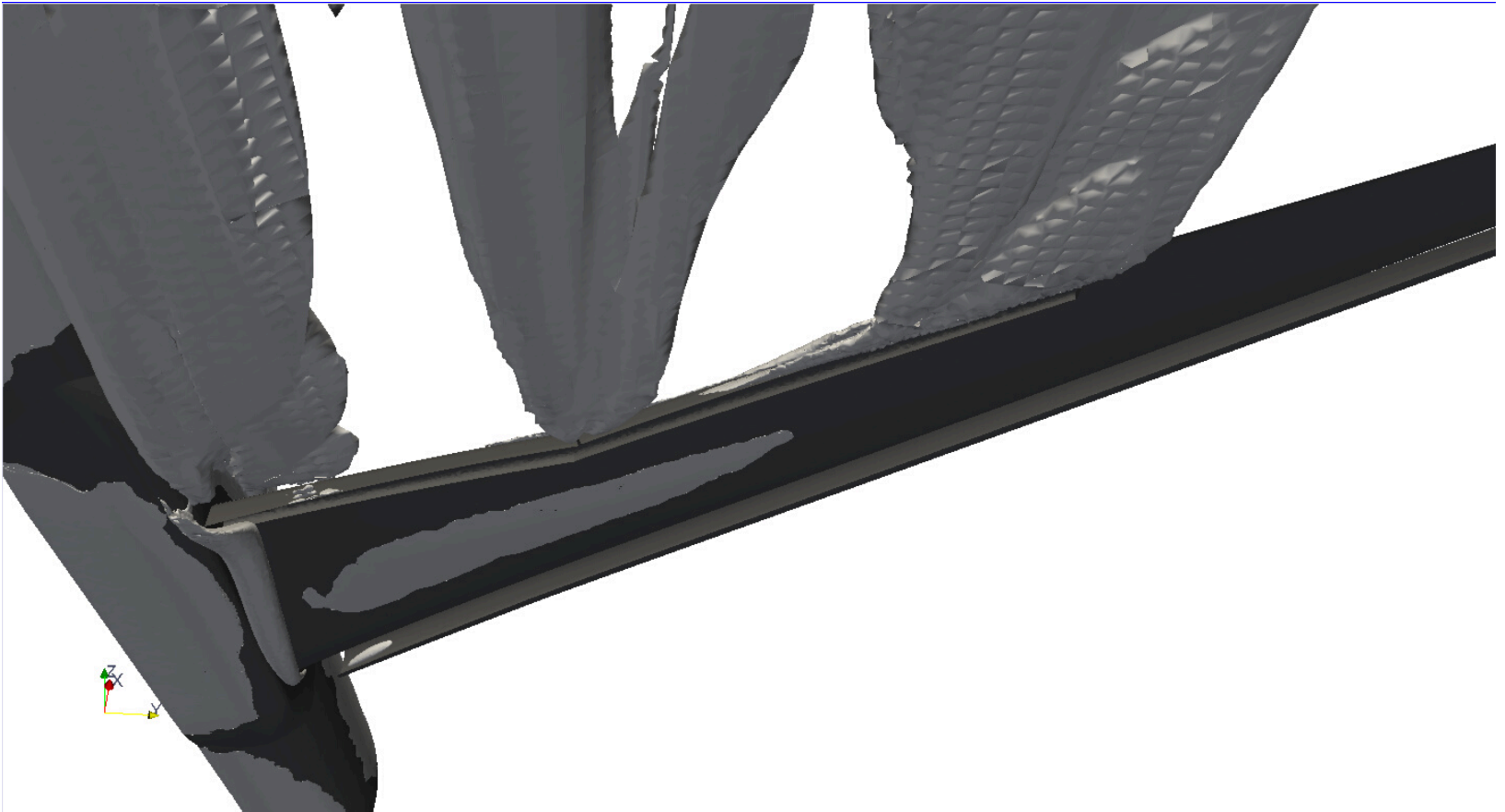
CRM Wall Shear Stress Streaks and Streamlines: Committee:Coarse:16



CRM Adaptation Envelope: Simmetrix:Coarse:16



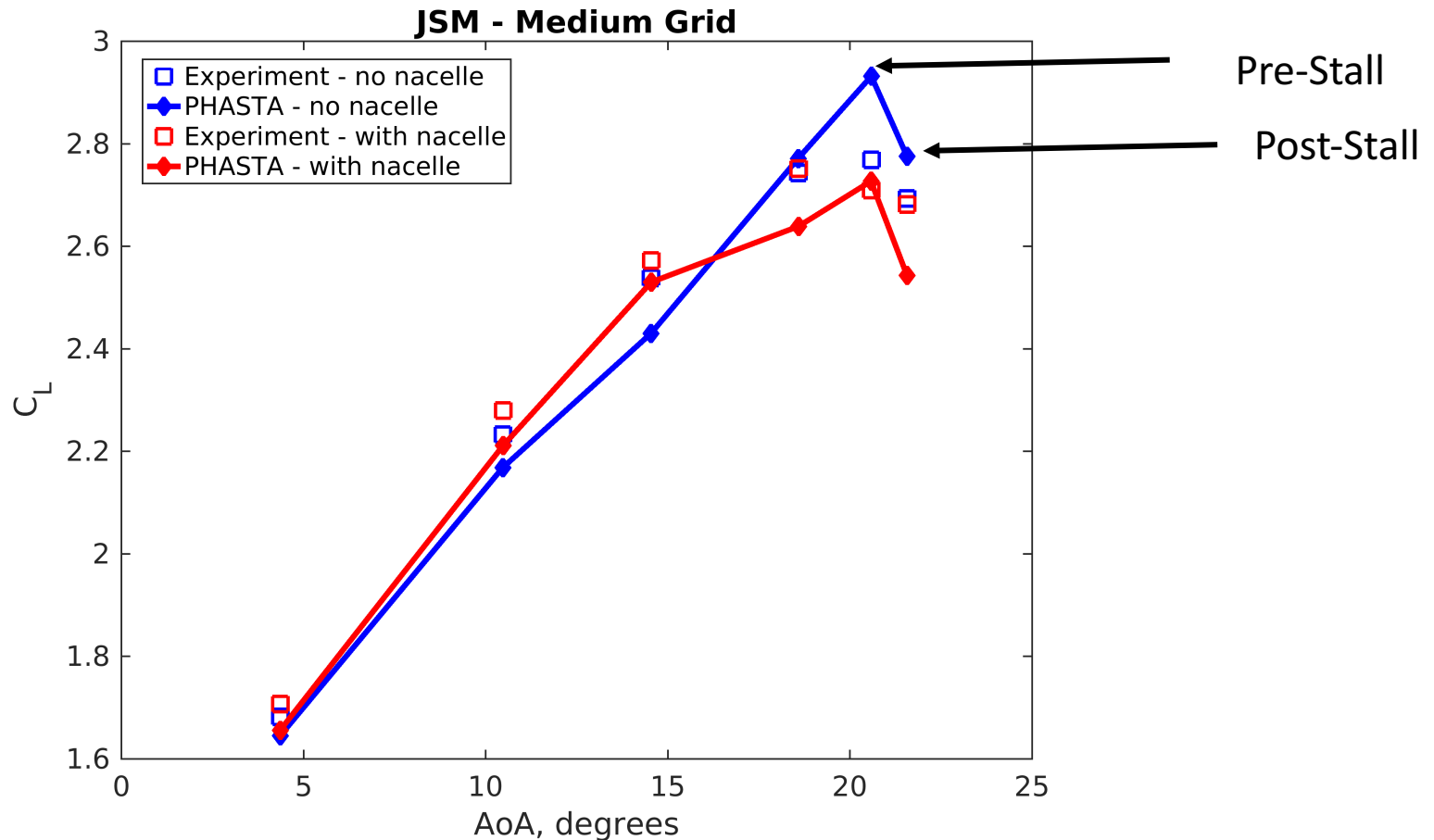
CRM Adaptation Envelope: Simmetrix:Coarse:16



JSM

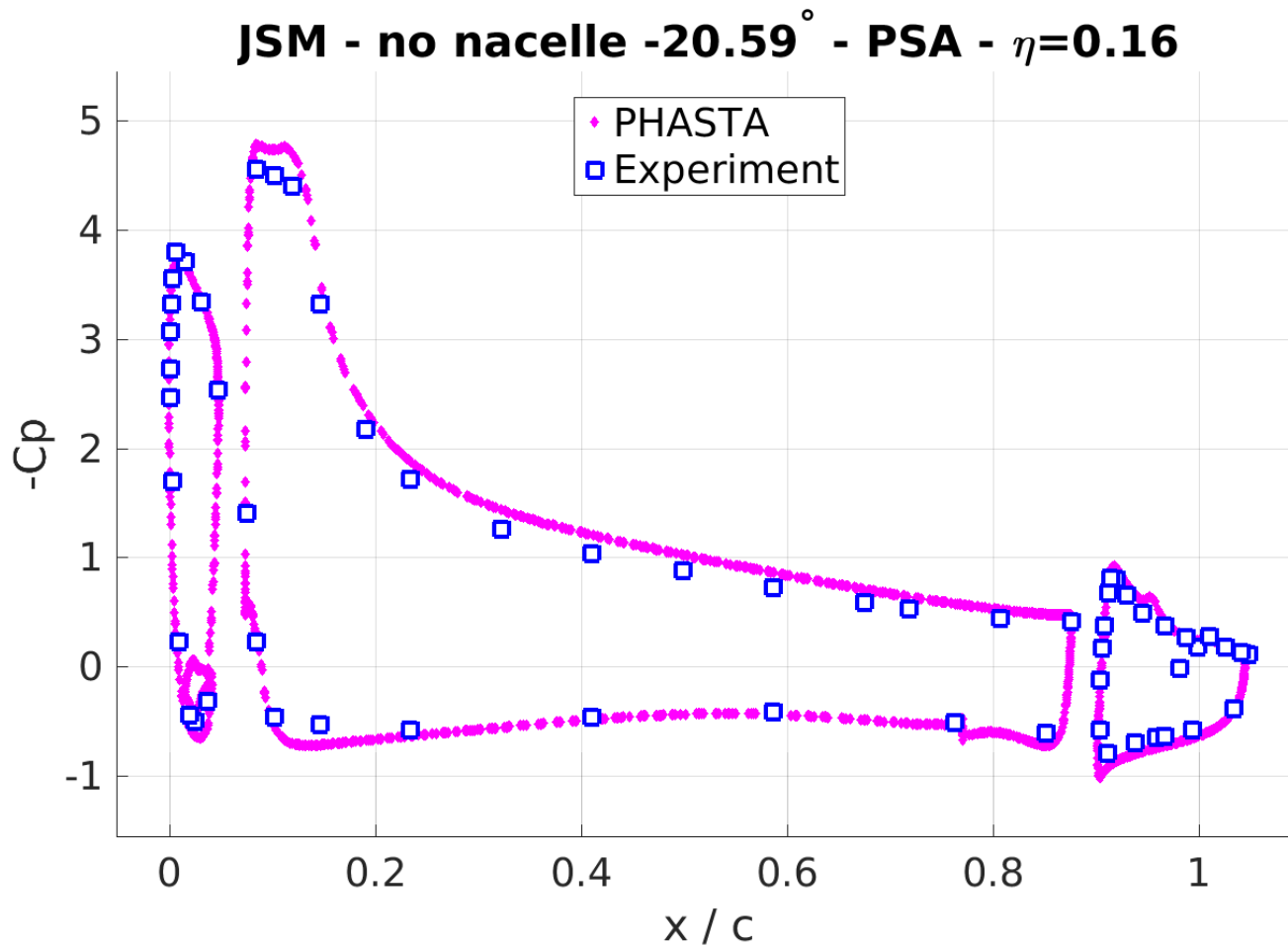
Aerodynamic forces

- Lift force
 - Stall angle predicted well but lift value off -- surprising given how well the C_p matches.
 - BUT, as with others, stall not the same mechanism as the experiment.
 - Influence of nacelle predicted well at lower AoA, not as much at larger angles.



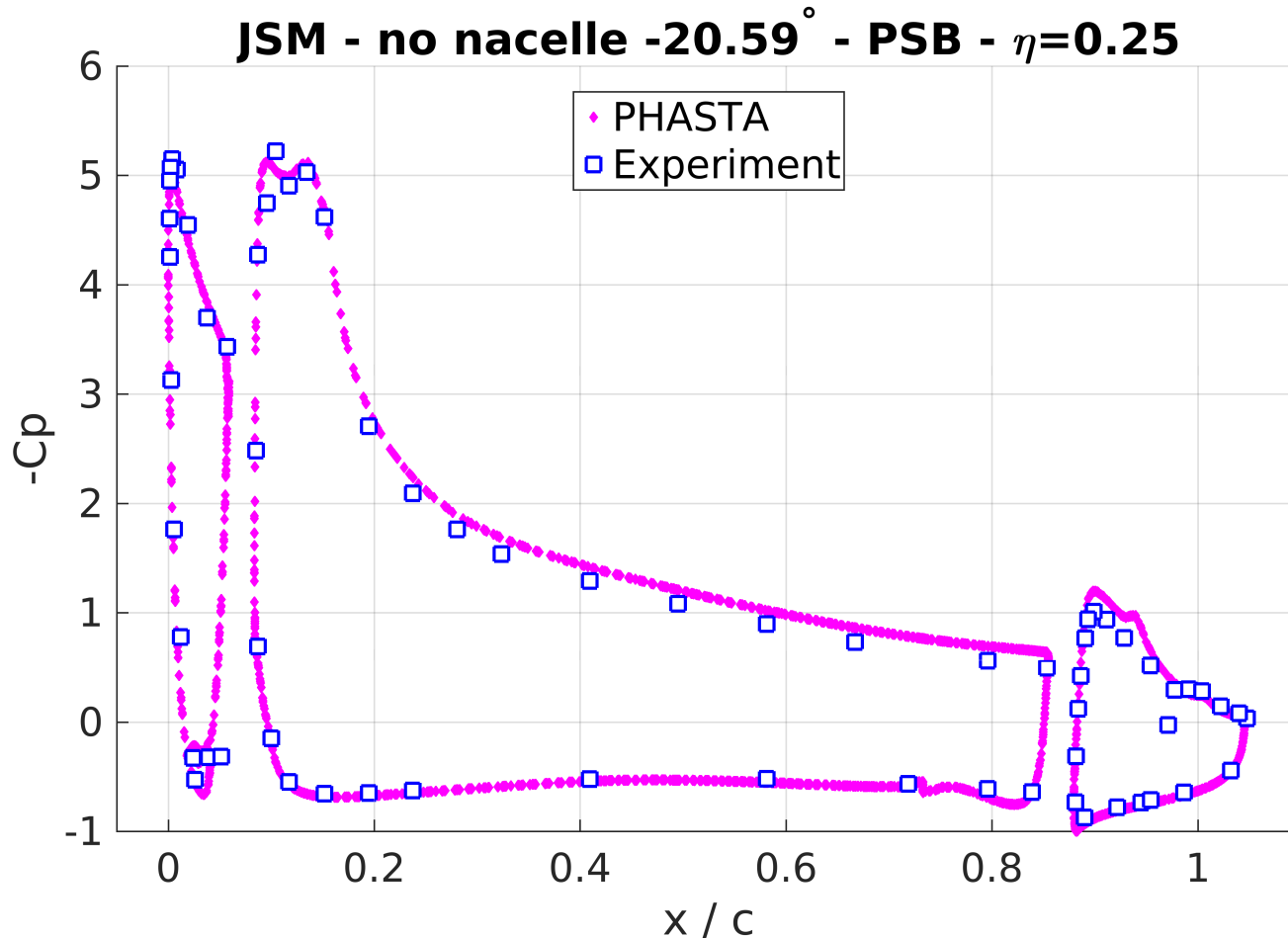
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Pressure Coefficients: Pre-Stall



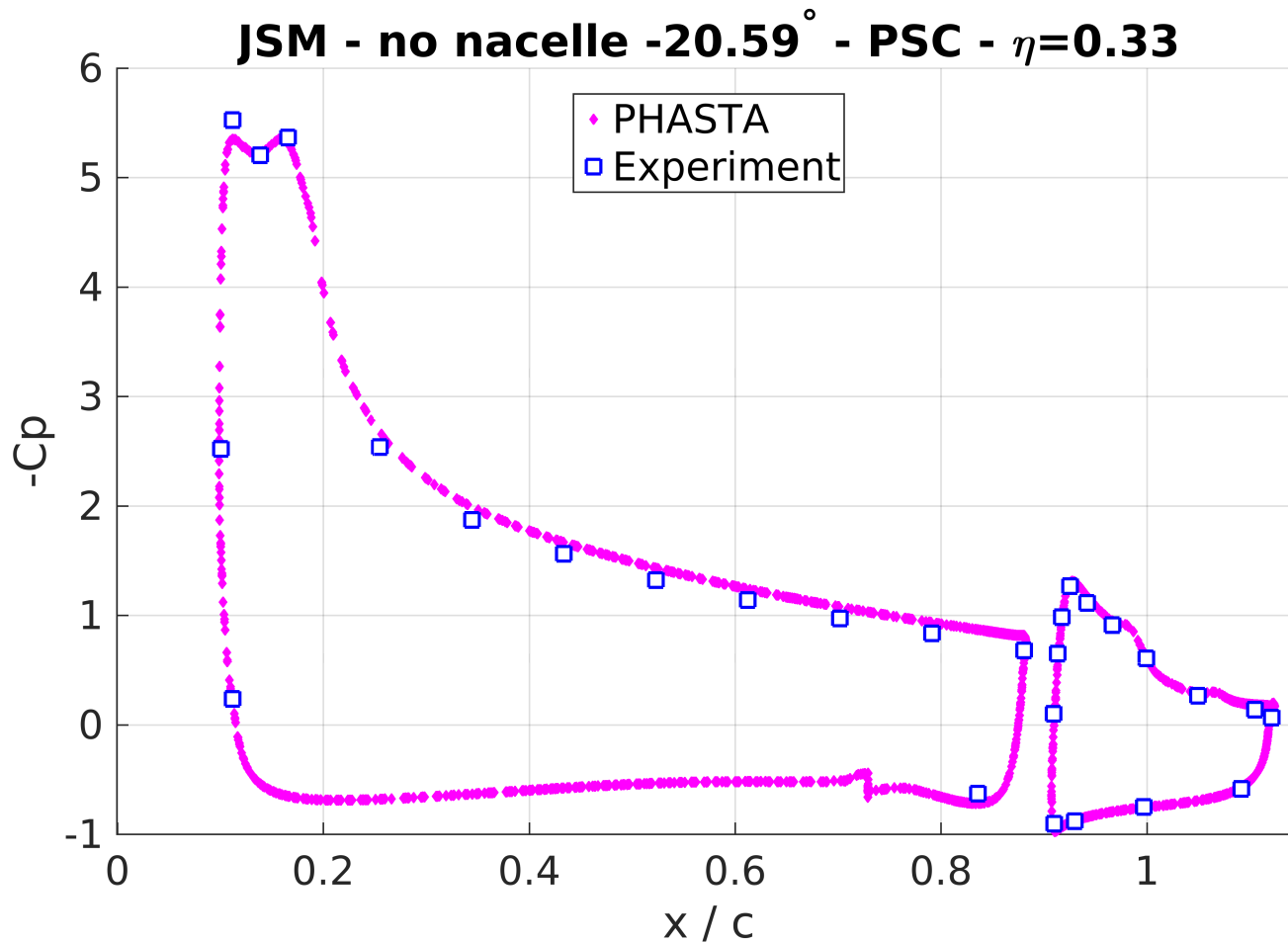
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Pressure Coefficients : Pre-Stall



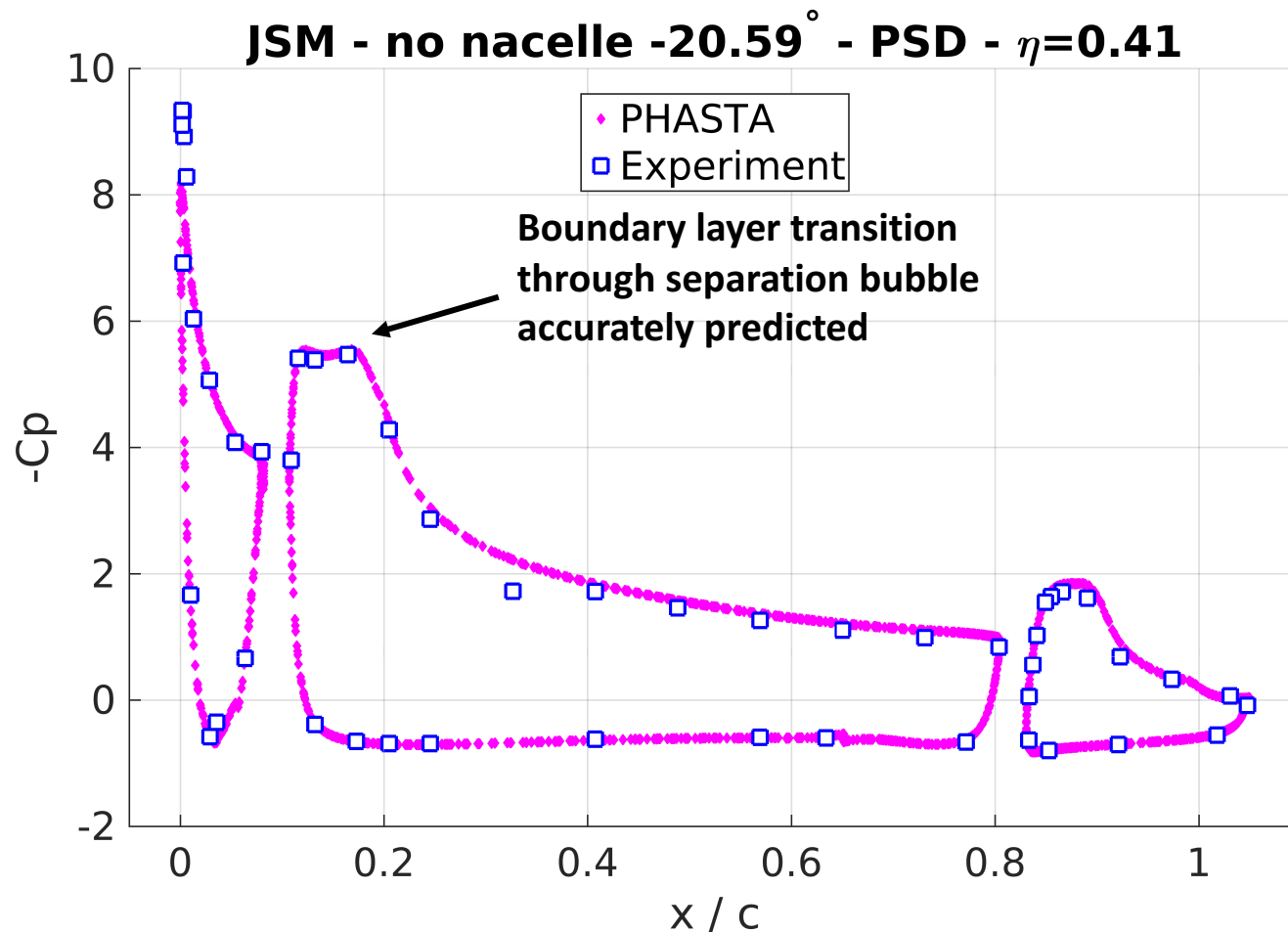
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Pressure Coefficients : Pre-Stall



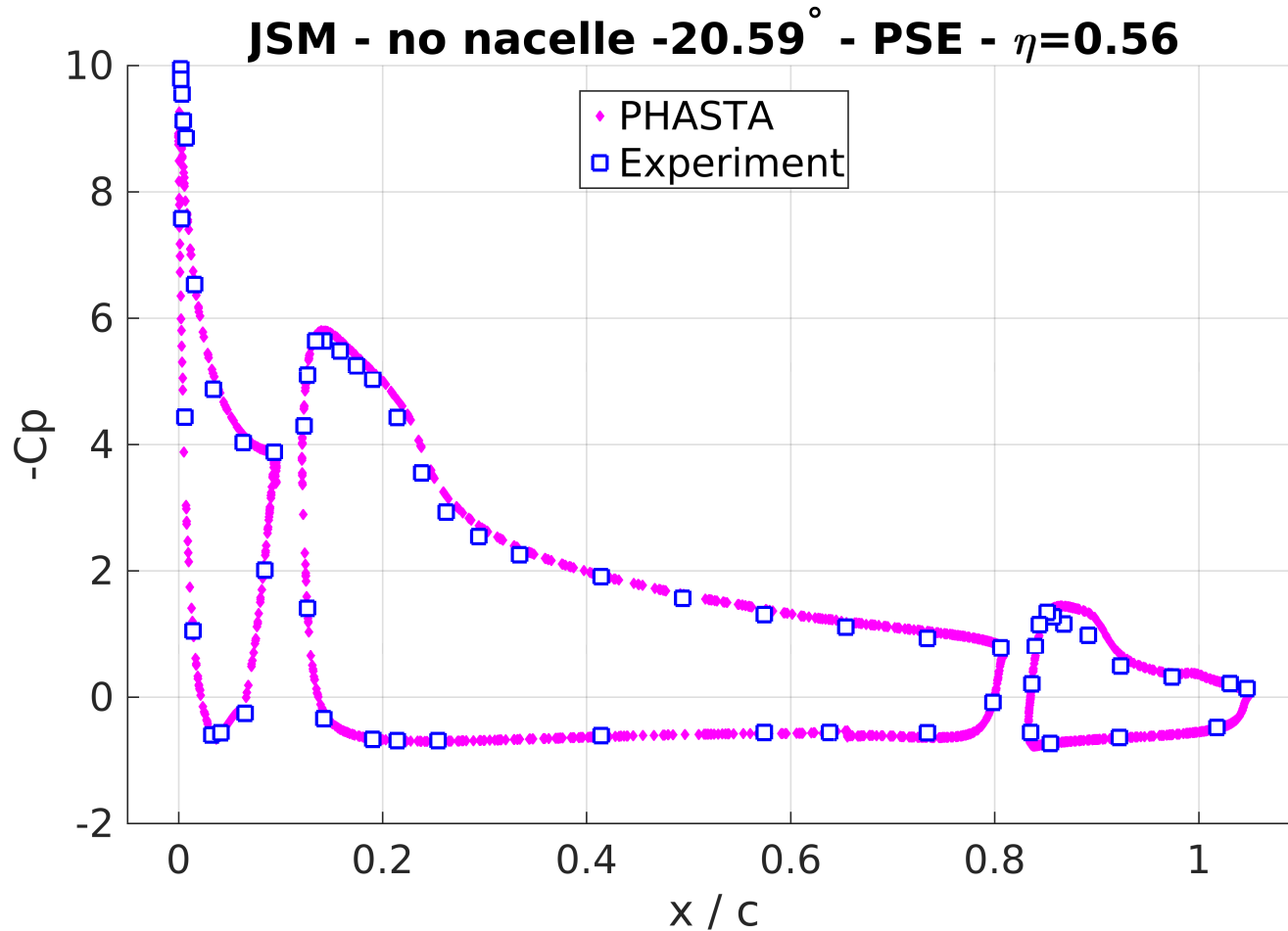
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Pressure Coefficients : Pre-Stall



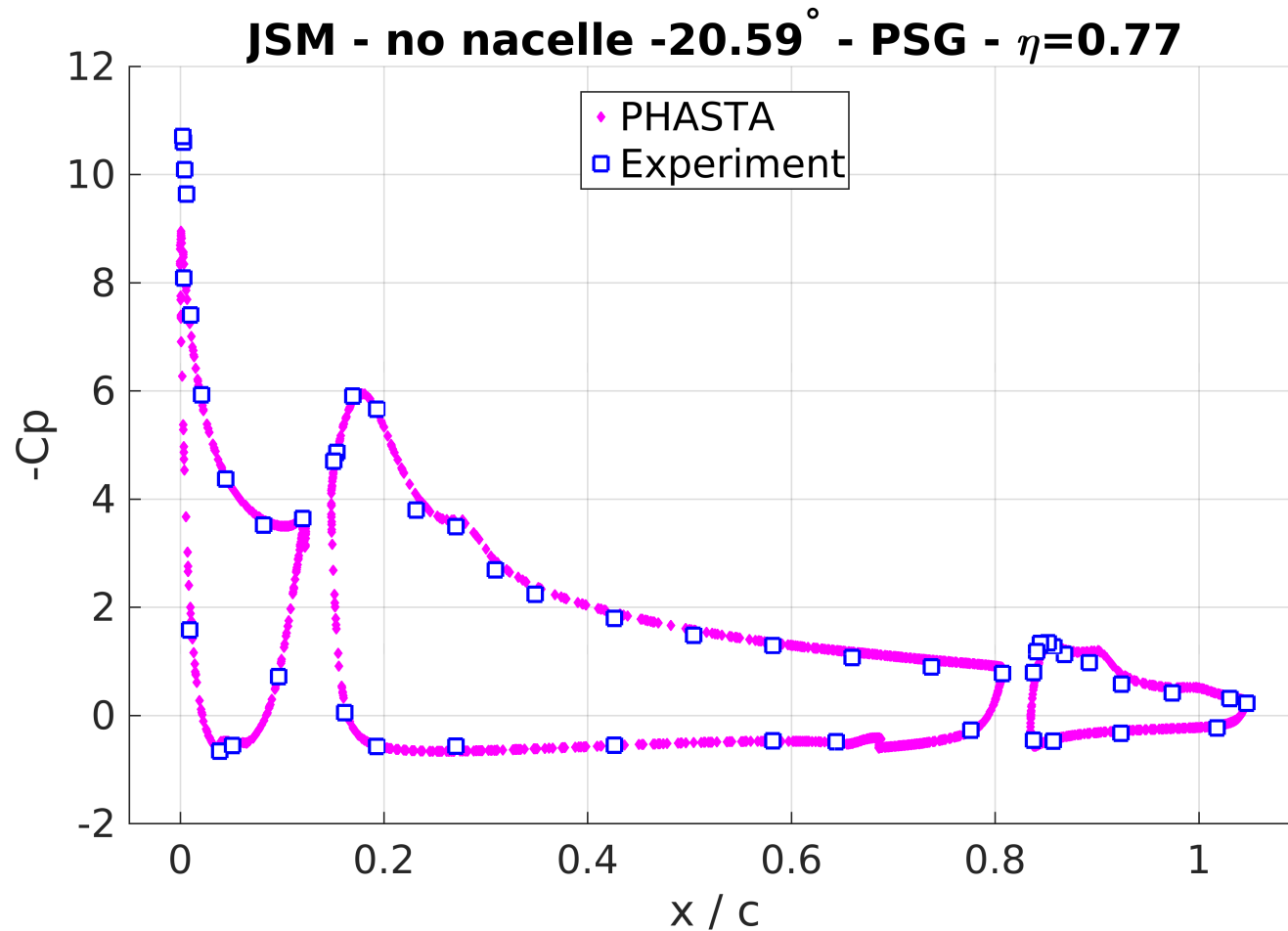
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Pressure Coefficients : Pre-Stall



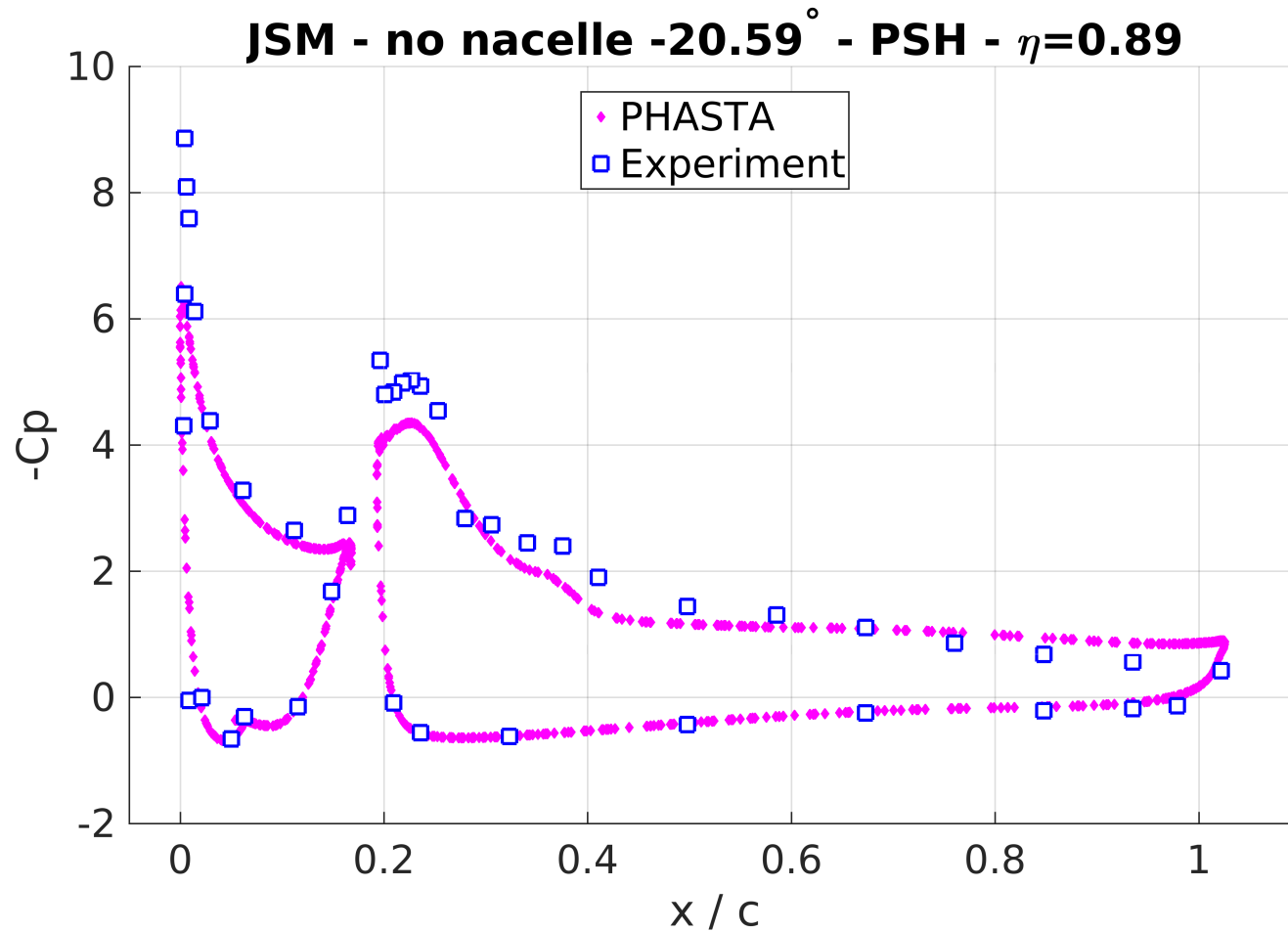
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Pressure Coefficients : Pre-Stall

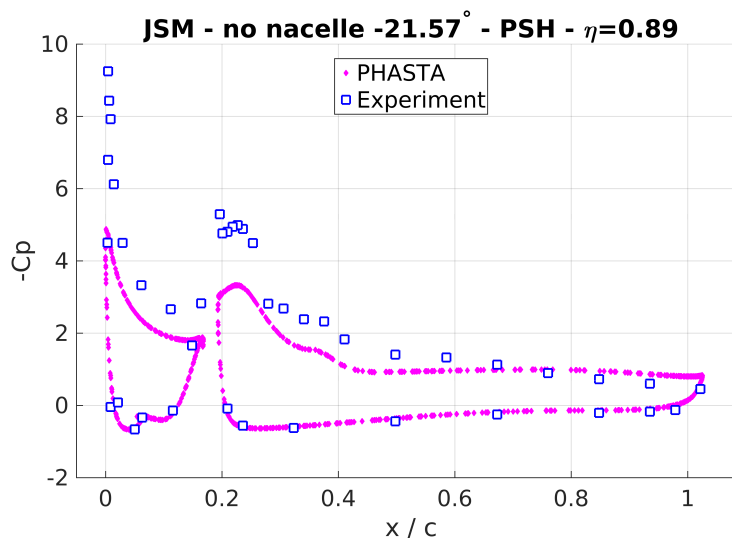
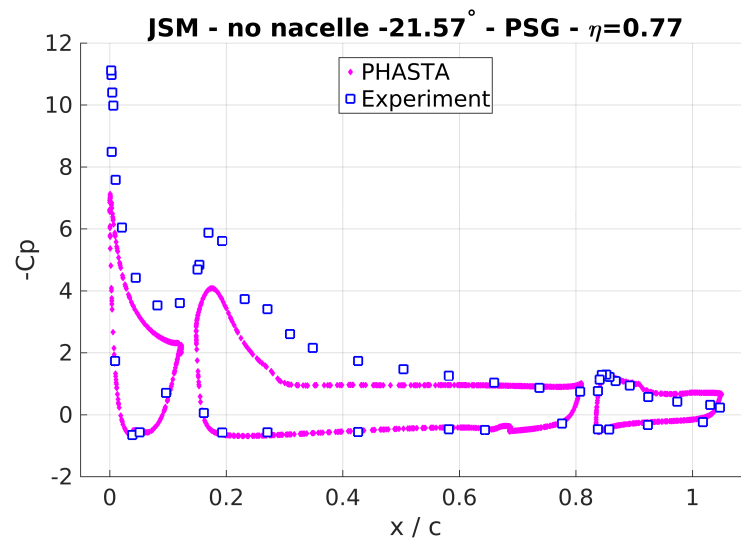
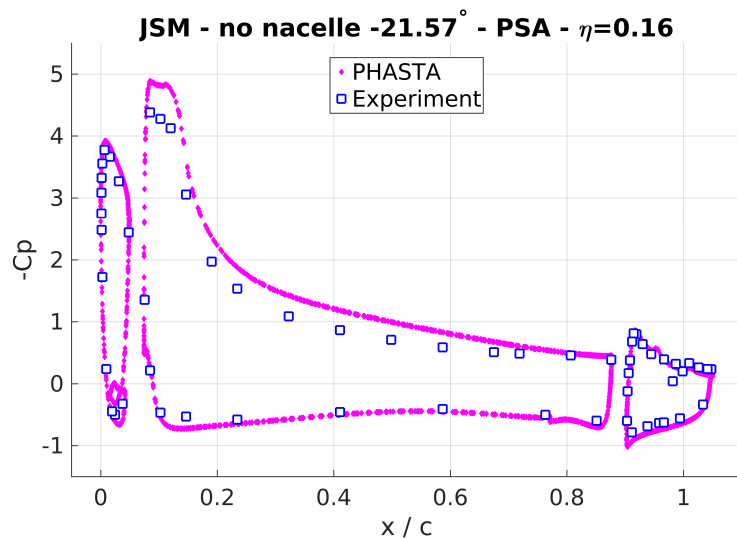


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Pressure Coefficients...and One Less Great

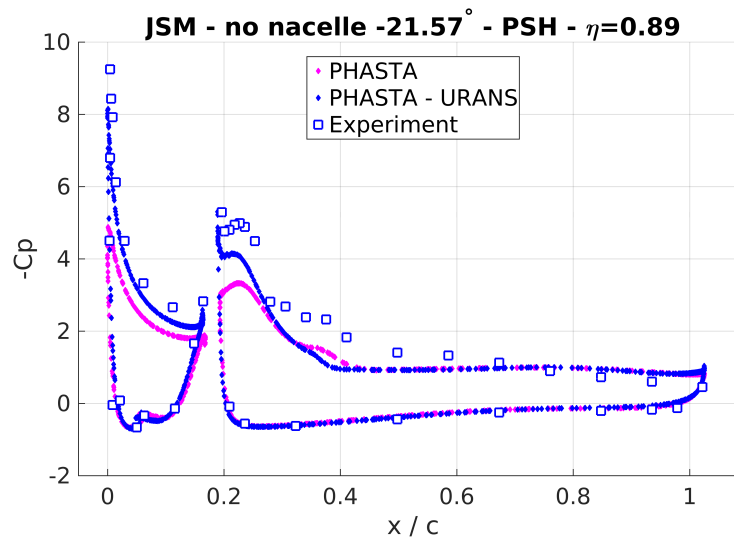
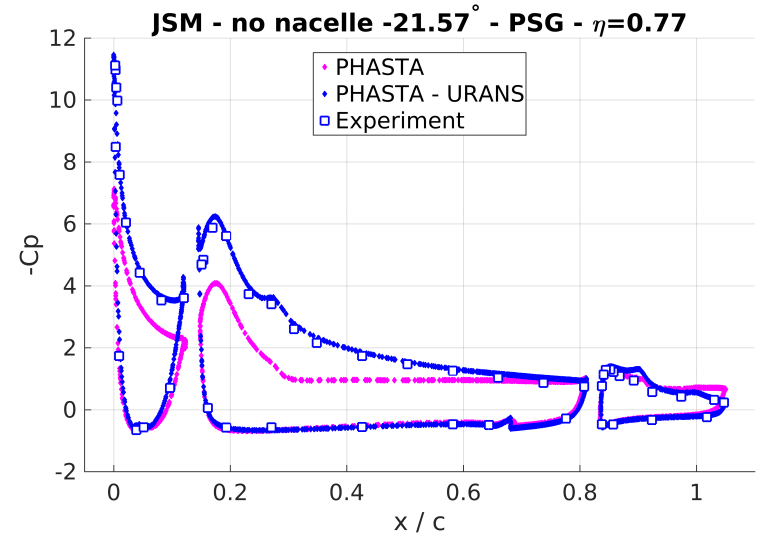
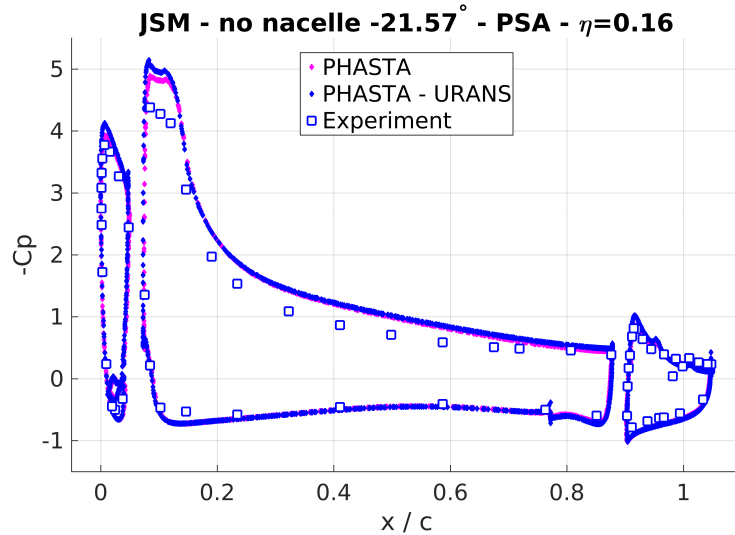


Pressure Coefficients: Post-Stall: Only the bad ones!



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Pressure Coefficients: Post-Stall: URANS Helps Some

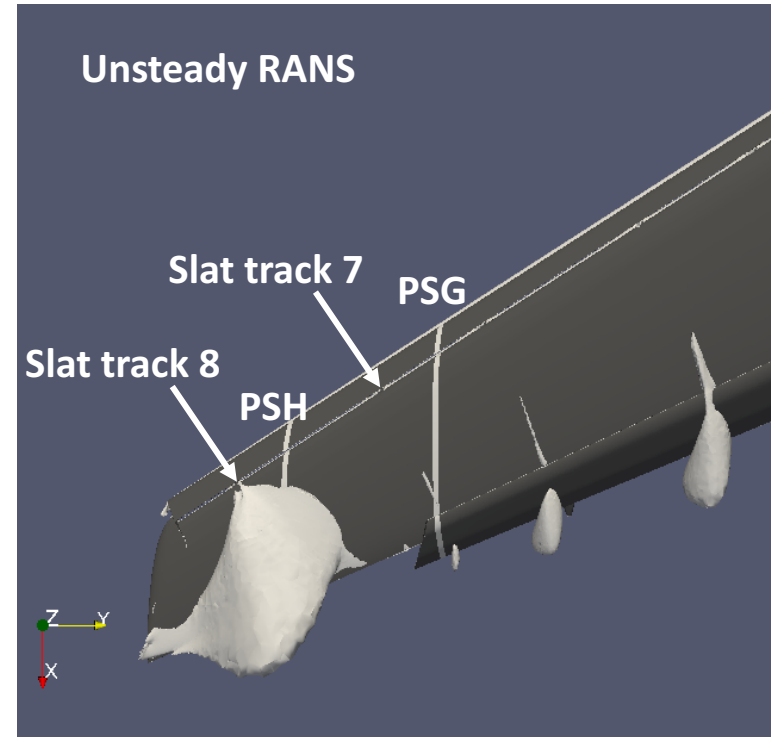
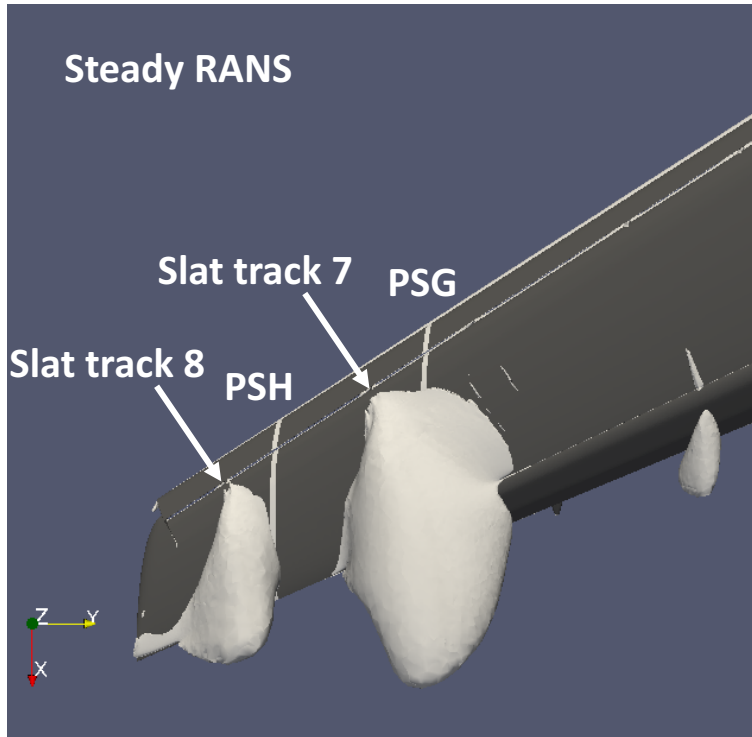


URANS $D_{tf}=Dt$
 $U/c=0.05$
0.01 no different.
URANS started
from uniform flow
IC.

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Velocity Isosurfaces: Post-Stall

- Steady RANS predicts massive separation regions at PSG and PSH
- These are caused by vortical structures shed by slat track 7 and 8
- URANS does not predict separation at PSG and has modified shape of separation region at PSH

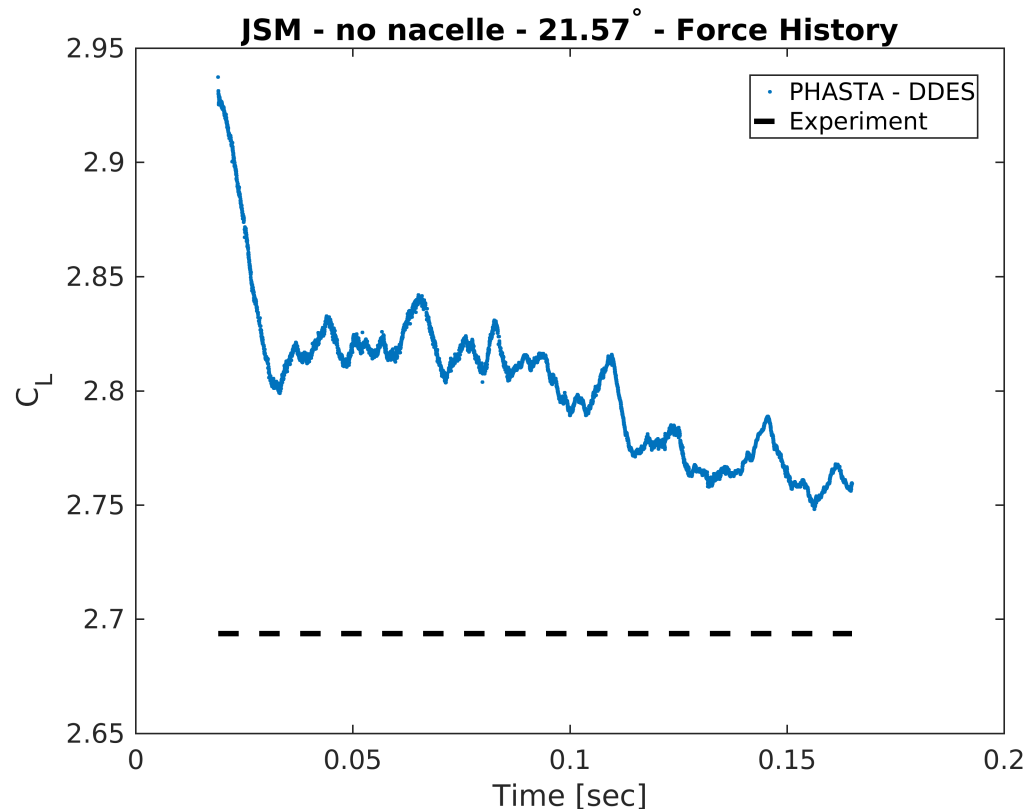


Isosurfaces of $\bar{u} = -0.1 \text{ m/s}$

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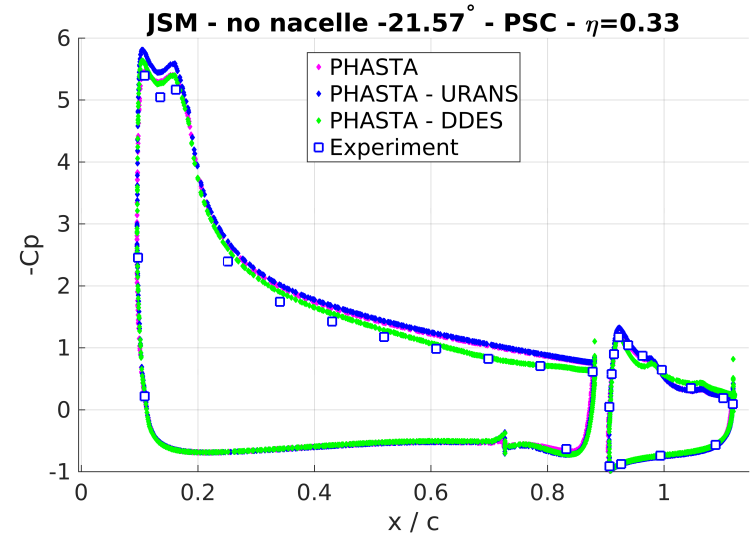
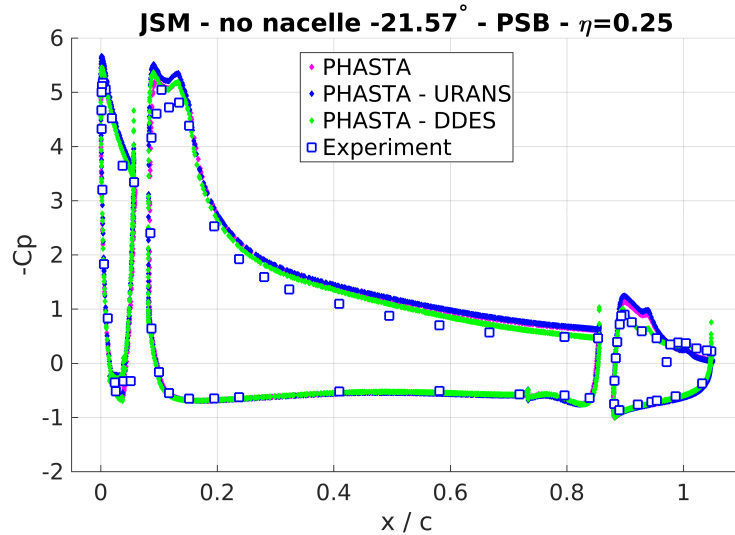
DDES Force: Post-Stall

- DDES simulation on C2 mesh still in progress. 15k steps=15 chord flights=.15 seconds,
- Lift coefficient approaching experimental value

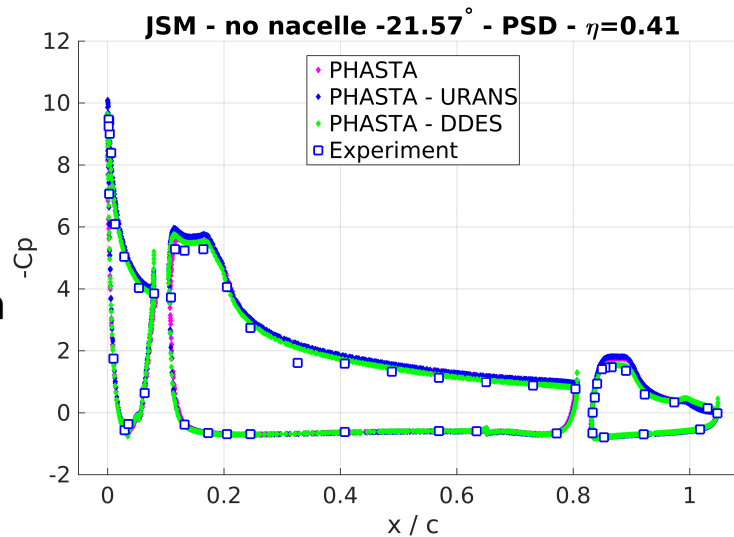


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DDES Pressure Profiles: Post-Stall

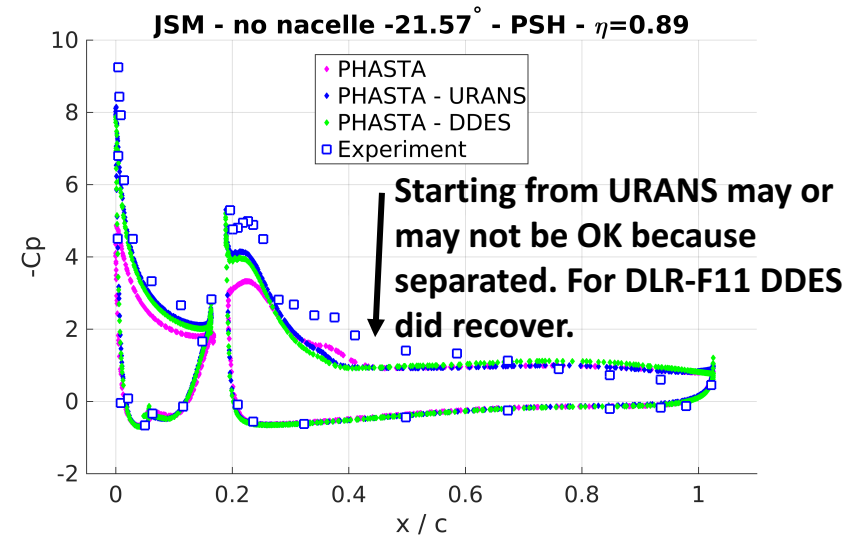
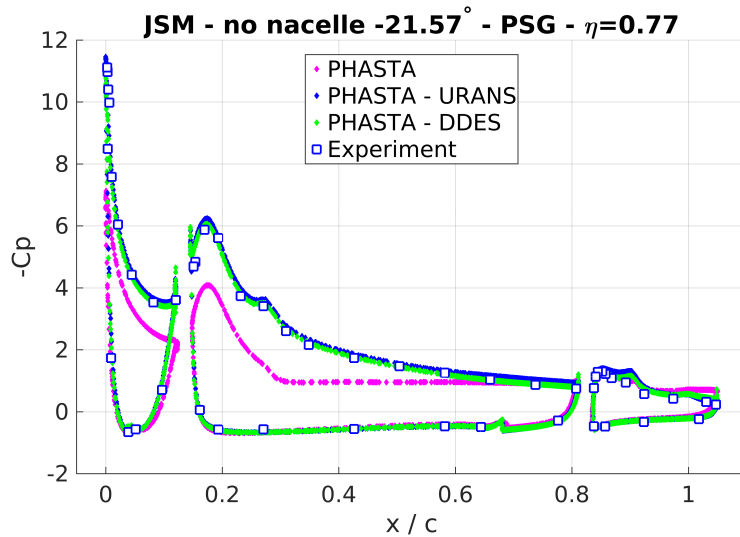
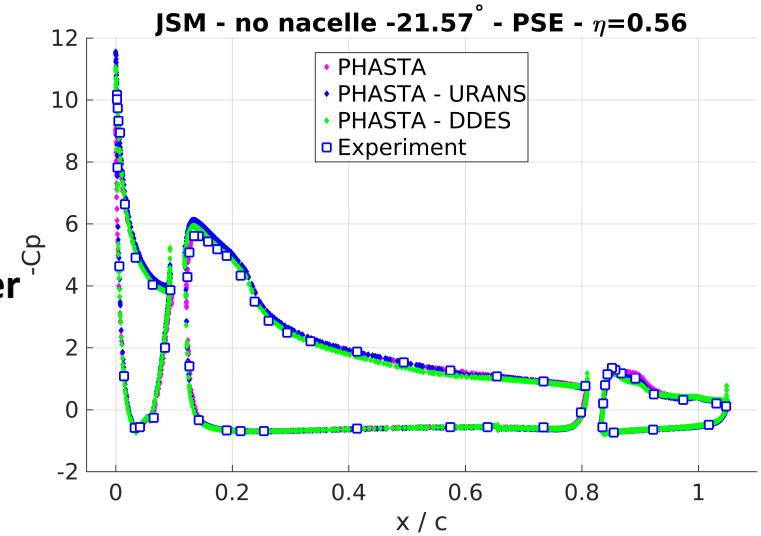
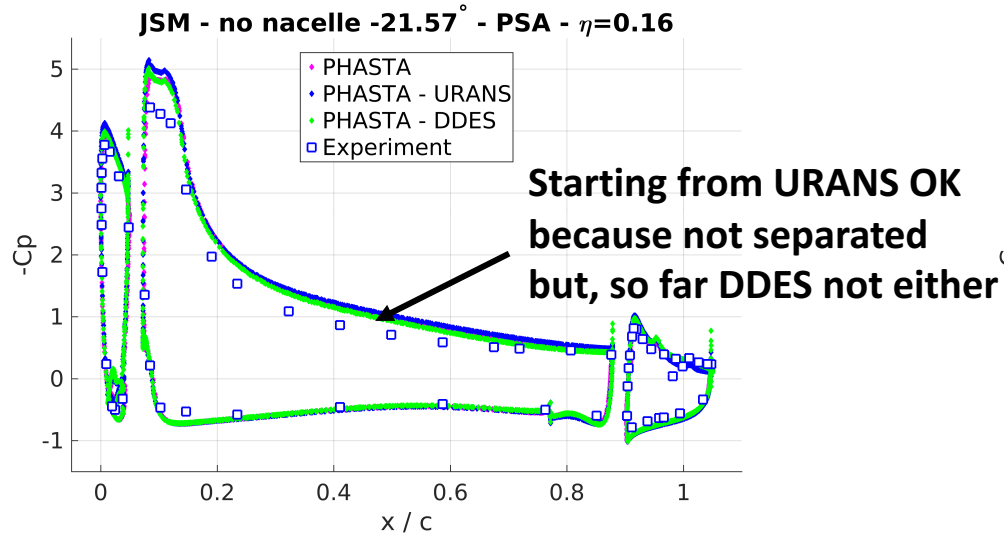


DDES gives a little better prediction over URANS of pressure at the TE of main element and over the flap



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DDES Pressure Profiles: Post-Stall



Summary

- CRM
 - Good convergence on committee (B1-C/M/F) and Simmetrix grids (C/M)
 - Simmetrix grid used medium wall-normal resolution and this seemed to improve coarse-grid lift prediction dramatically
 - Adaptations of Simmetrix coarse grid ongoing
- JSM (2-c also completed and submitted but no time to discuss) 2-a:
 - RANS (Steady)
 - Pre-Stall C_p predictions excellent for $h \leq 0.77$, premature separation for $h = 0.89$
 - Post-stall C_p $h = 0.77$ separated: separation from outboard, not capturing experiment inboard separation—correct max lift angle/stall, wrong reason.
 - URANS
 - Able to improve $h = 0.77$ but $h = 0.89$ still too separated, and missing root separation.
 - DDES
 - Ongoing....trending towards improved outboard prediction.
 - Likely require adaptivity to get root separation and $h = 0.89$ correct.
 - DLR-F11 was successful but it was a more DDES friendly mesh (less anisotropic).
- Acknowledgments: ALCF INCITE and Early Science Projects for Mira and Theta -- DOE Office of Science Contract DE-AC02-06CH11357; Janus and Summit supercomputers – NSF CNS-0821794 and ACI-1532235 and ACI-1532236. Software components: Simmetrix, SCOREC, Altair, Kitware.

Thanks!